



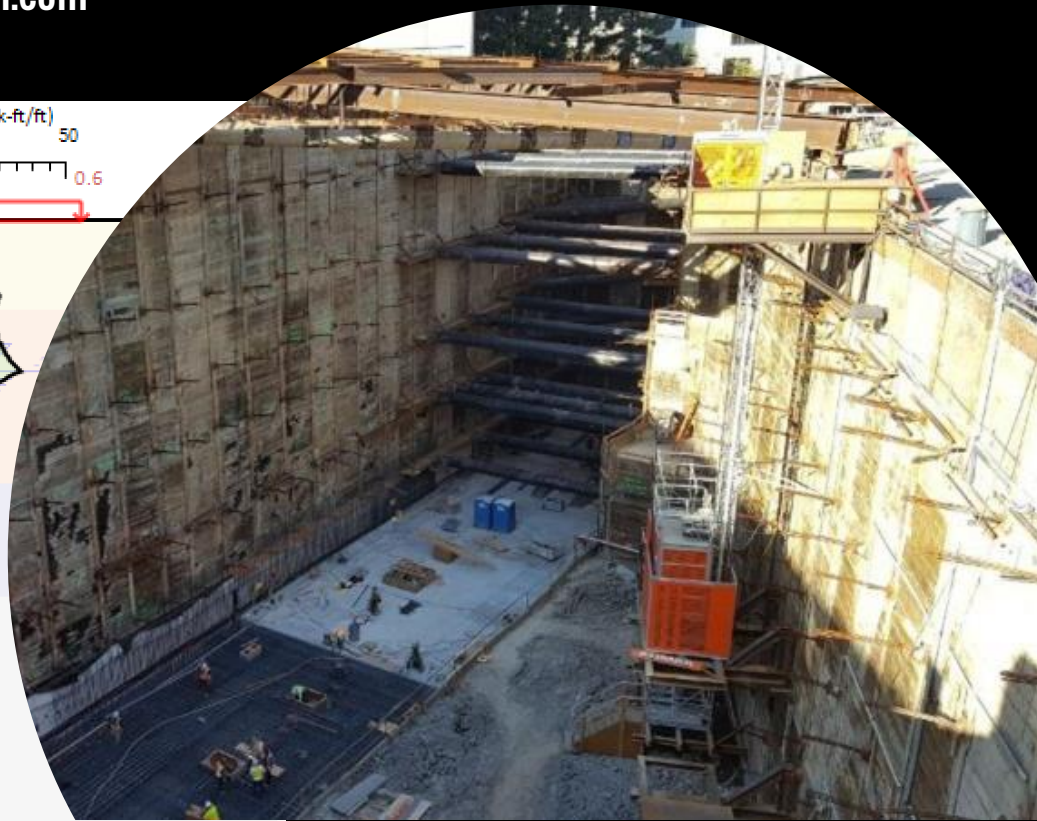
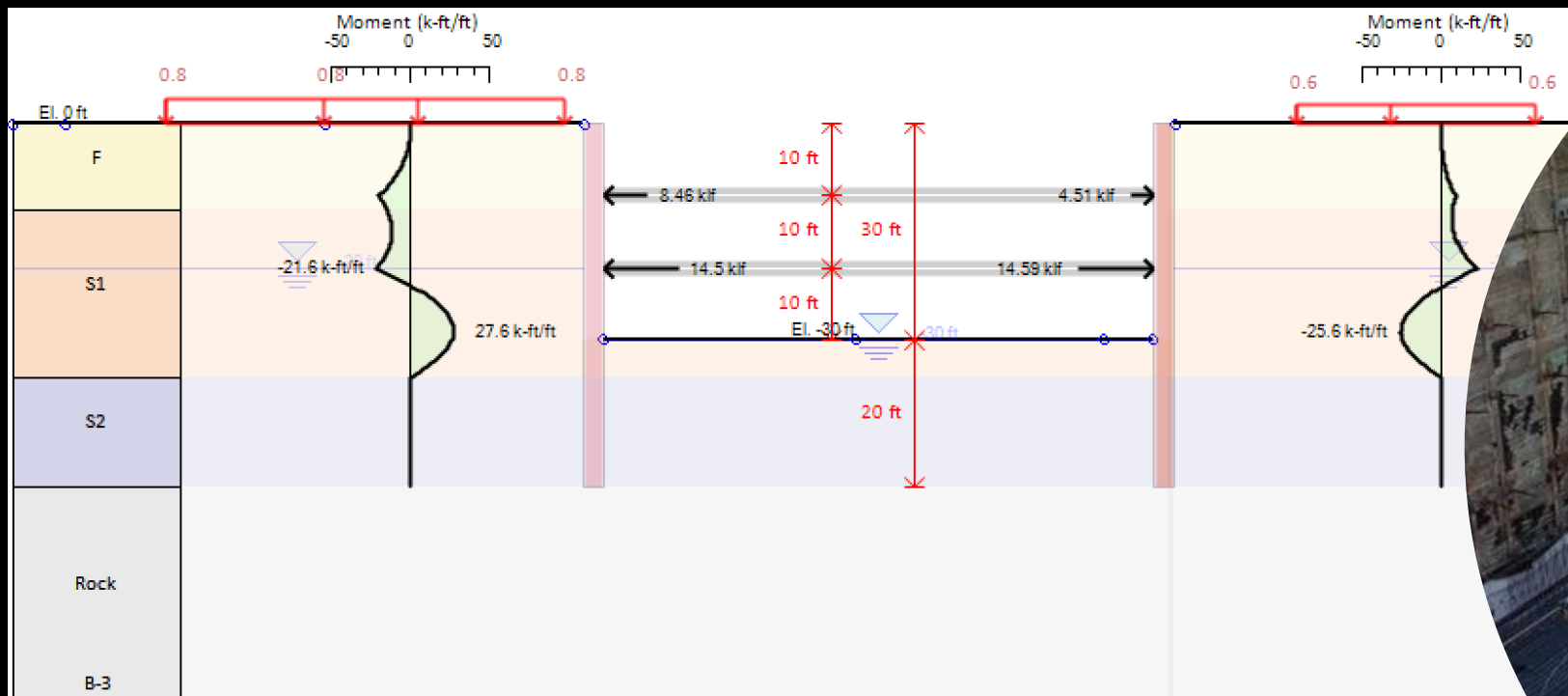
DeepEX
Shoring Design
Software



DEEP EXCAVATION
GEOTECHNICAL SOFTWARE & SOLUTIONS

Design of Deep Excavations

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CEO Deep Excavation LLC
E: dimitrios@deepexcavation.com



Introduction

How we got started in deep excavations!



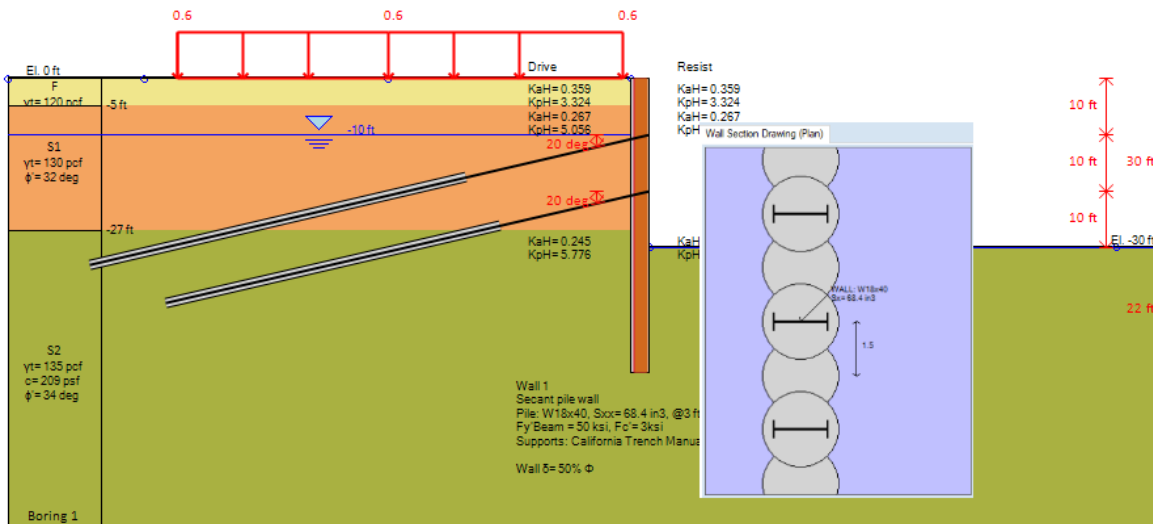
Exhibit 2: Excavation at World Trade Center Liberty & Greenwich, 1968

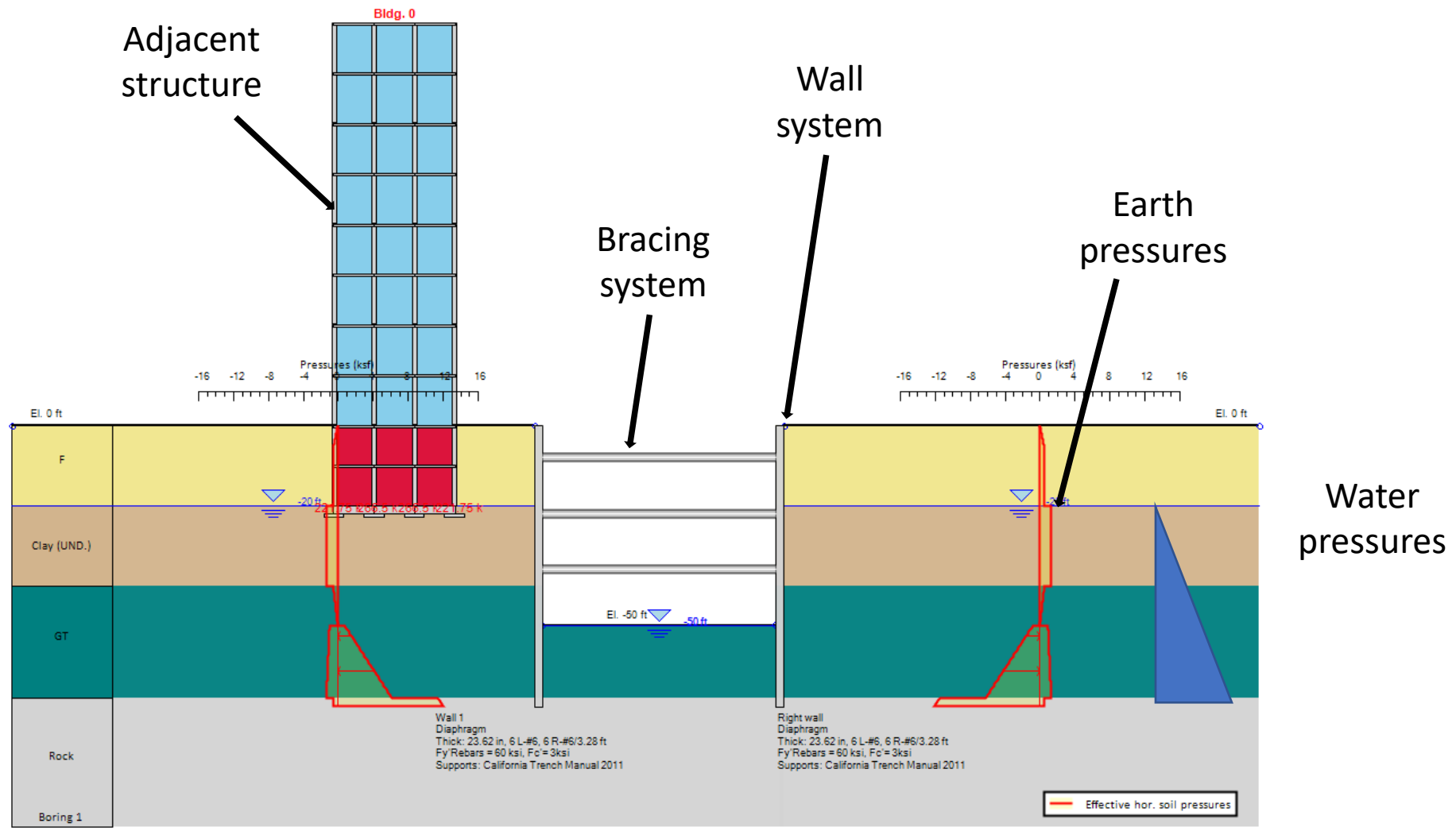


Exhibit 1: World Trade Center Bathtub and Original Conditions (adapted from NY Times 9/18/01)

Deep Excavation: Excavation deeper than 10 ft, that requires structural support.

- A deep excavation system has to retain earth, water, and neighboring structures
- Unknown factors and risks
- Soil properties estimation
- Protect adjacent properties
- Design issues and Code issues
- Economy
- Constructability







Retaining wall collapse on May 12, 2005



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Soldier pile walls



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Internal bracing - Subway Station



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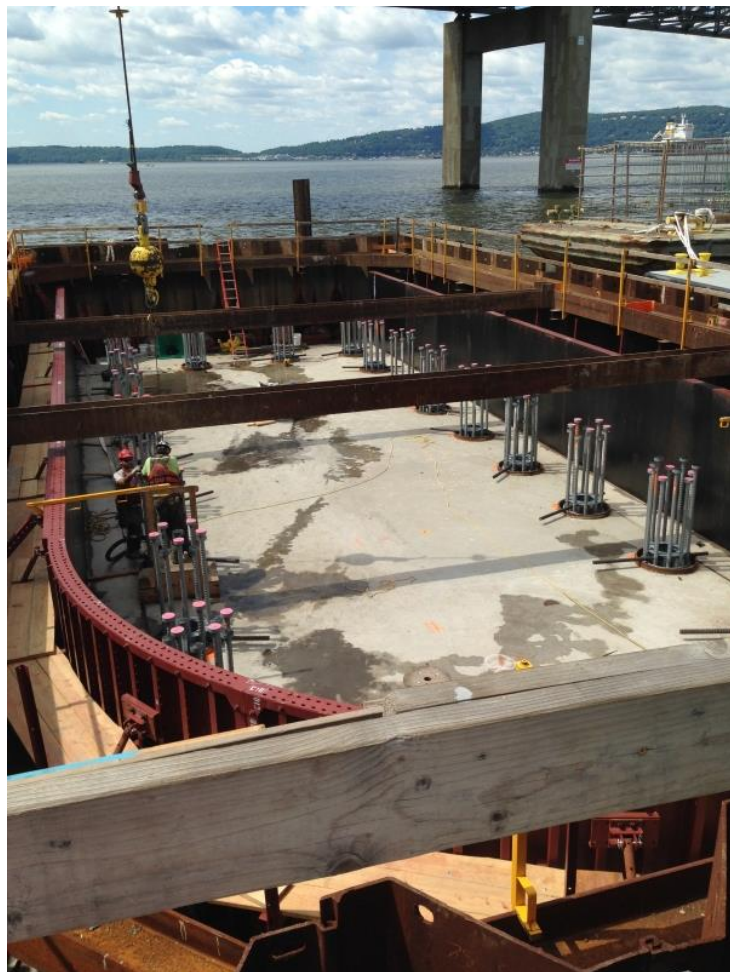




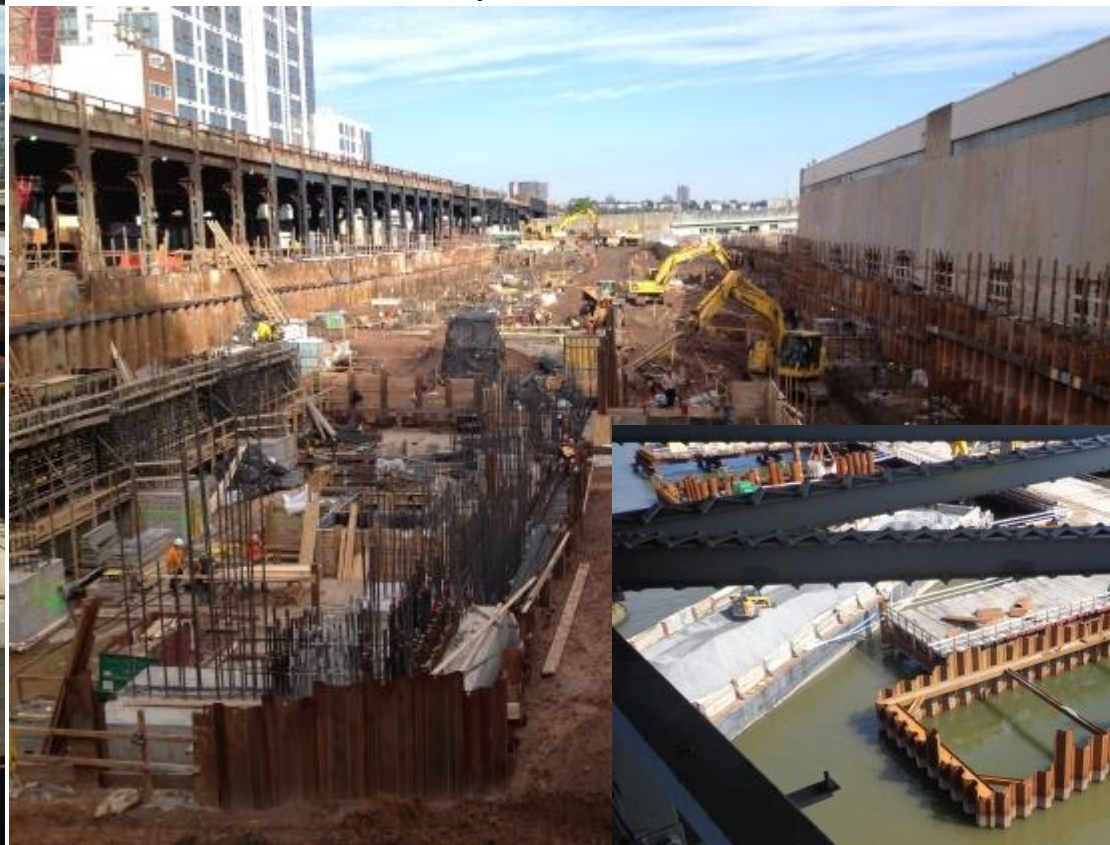
Cofferdams - sheet piles



Courtesy: FNA Associates



Courtesy: Siefert Associates



Courtesy: Siefert Associates



Secant pile walls - circular shafts



Courtesy: Hayward Baker



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Diaphragm walls



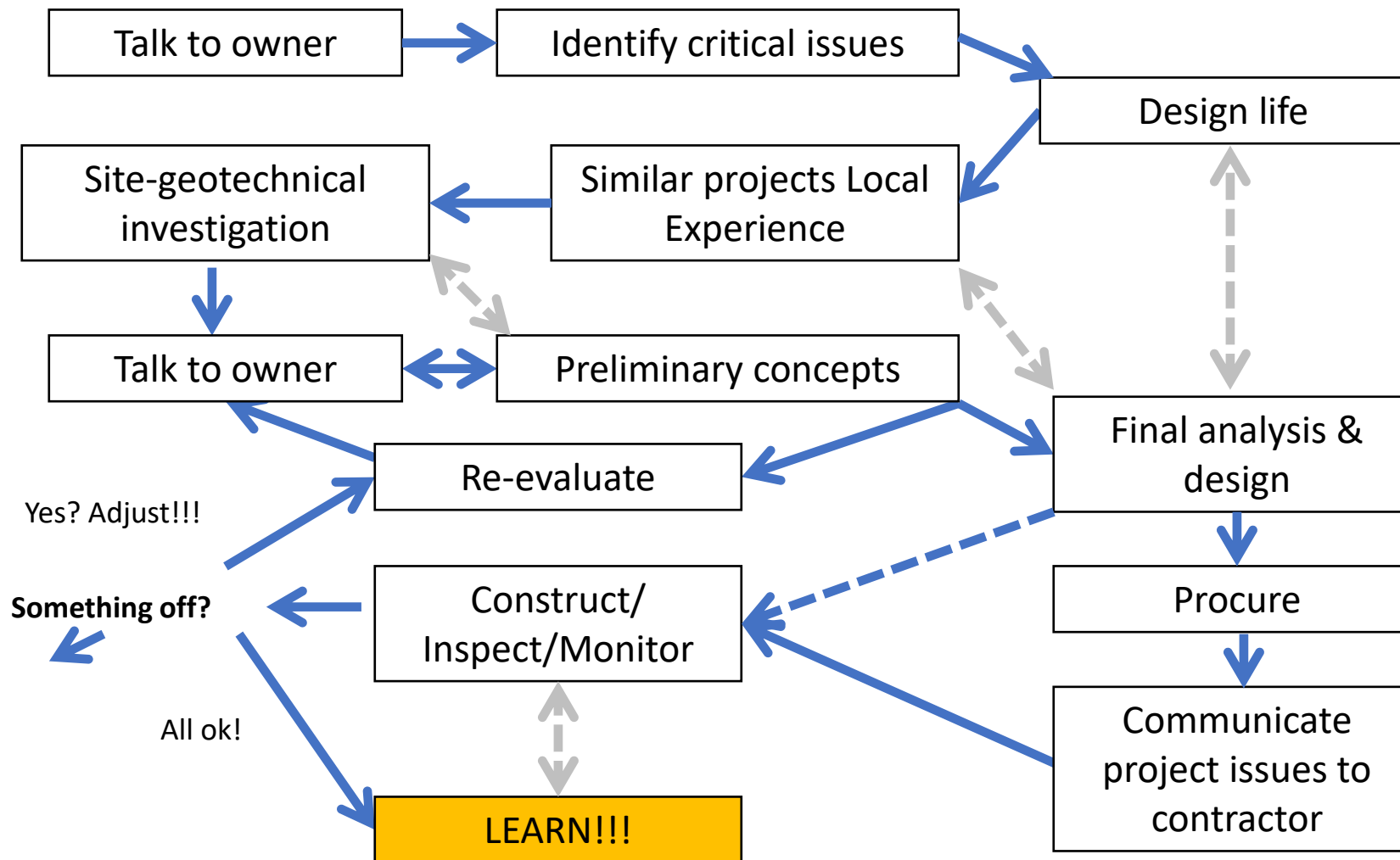
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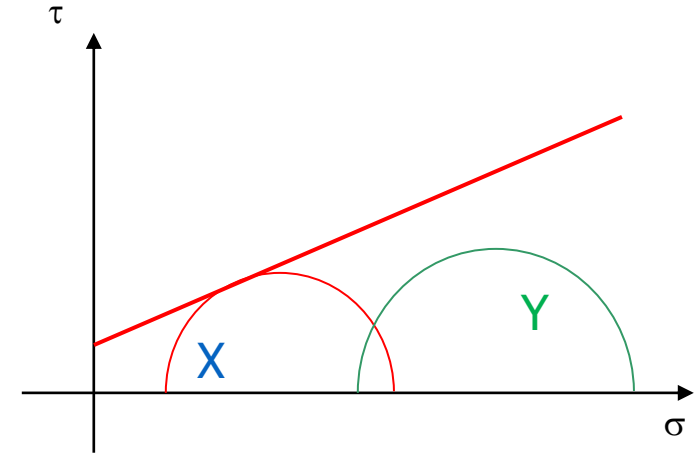
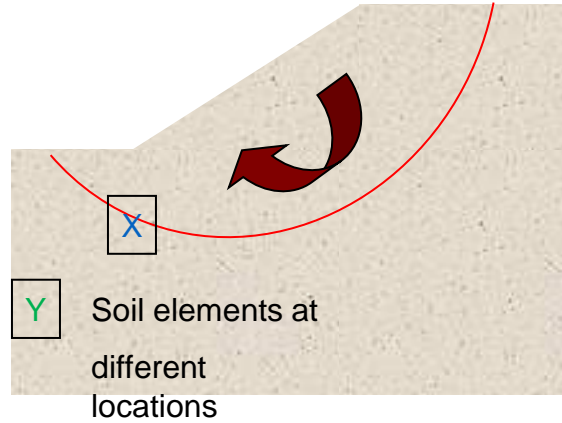


Soil, rock, water, and what's in place

- Soil variability
- Soil strength, drained-undrained
- Water conditions
- Thin-layers
- Collapsible soils
- In-situ vs. laboratory tests
- Consolidation settlements
- Obstructions
- Unforeseen conditions
- Fake geotechnical reports
- Overly conservative data
- Living on the edge?
- Water flow
- Groundwater drop down
- Contamination
- Utilities
- Existing structures

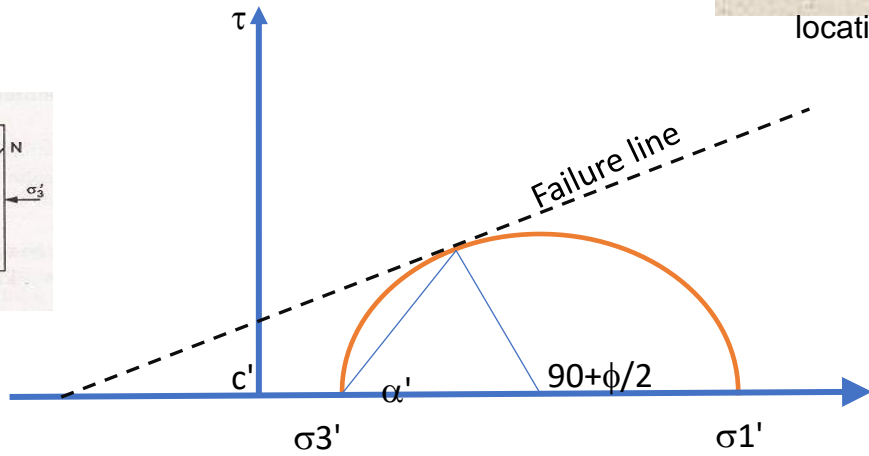
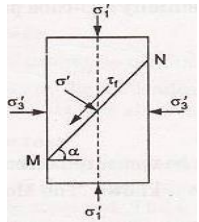


- Sands, silts, rocks, IGM
 - Use c' and ϕ'
- Clays in general:
 - Drained : c' and ϕ
 - Undrained: S_u
 - Look at default response



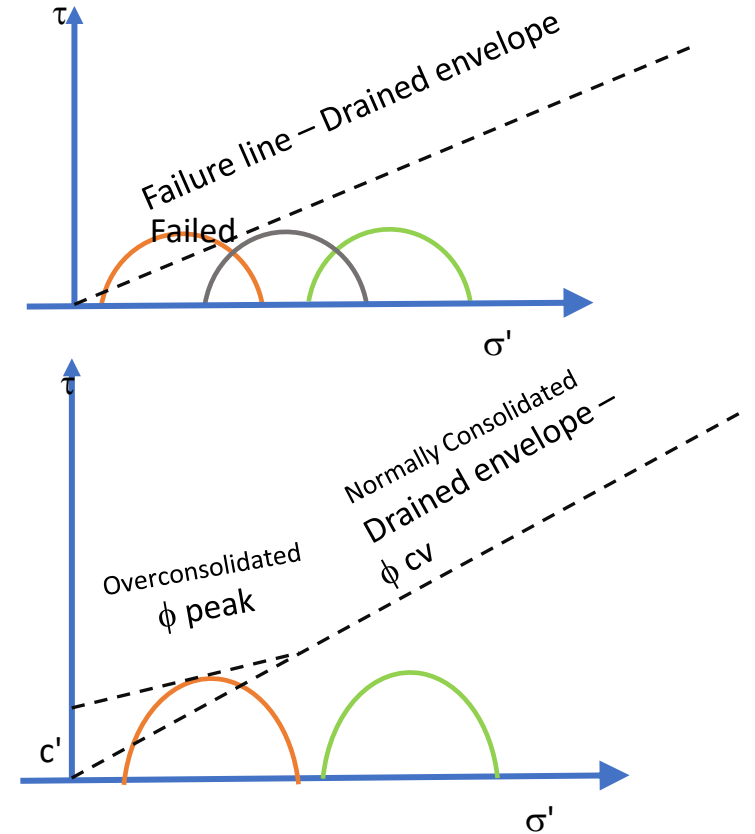
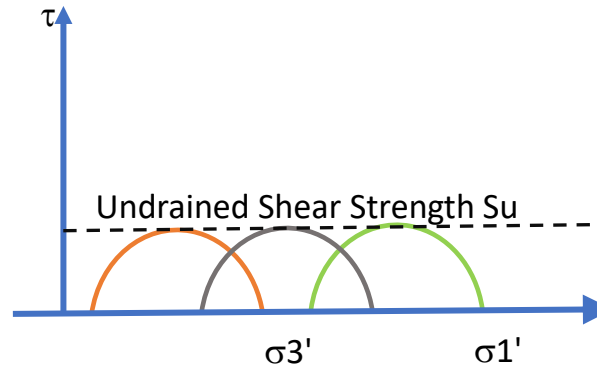
X ~ failure

Y ~ stable



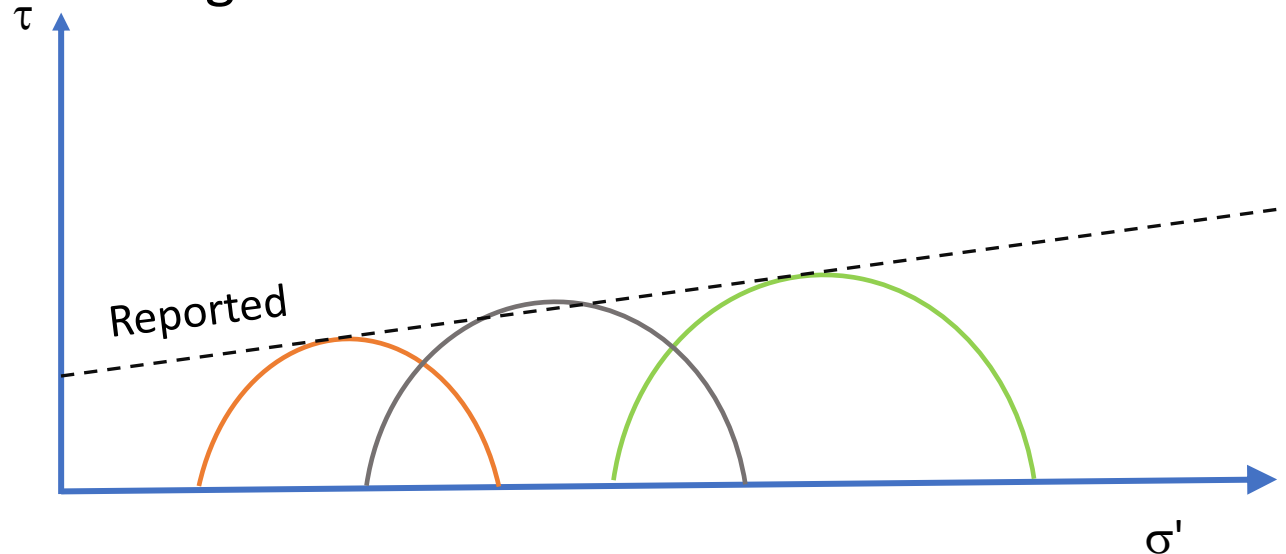
$$\tau = c' + \sigma' \tan(\phi)$$

- Clays undrained response
 - “Quick” stress change
 - Must be close to full saturation
 - Excess pore pressures



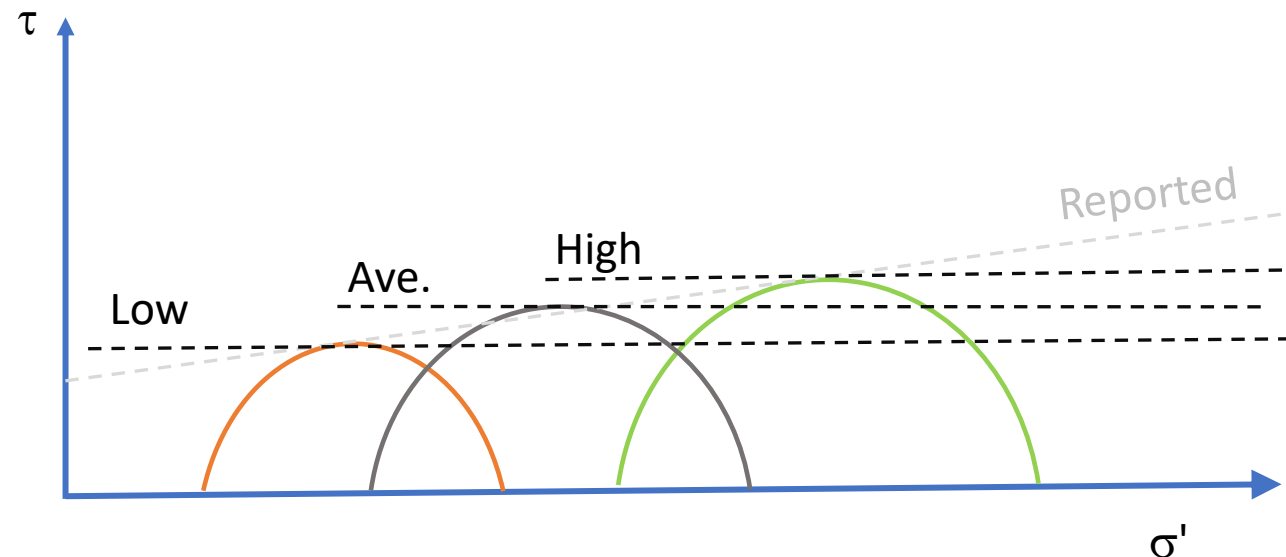
Clay Example

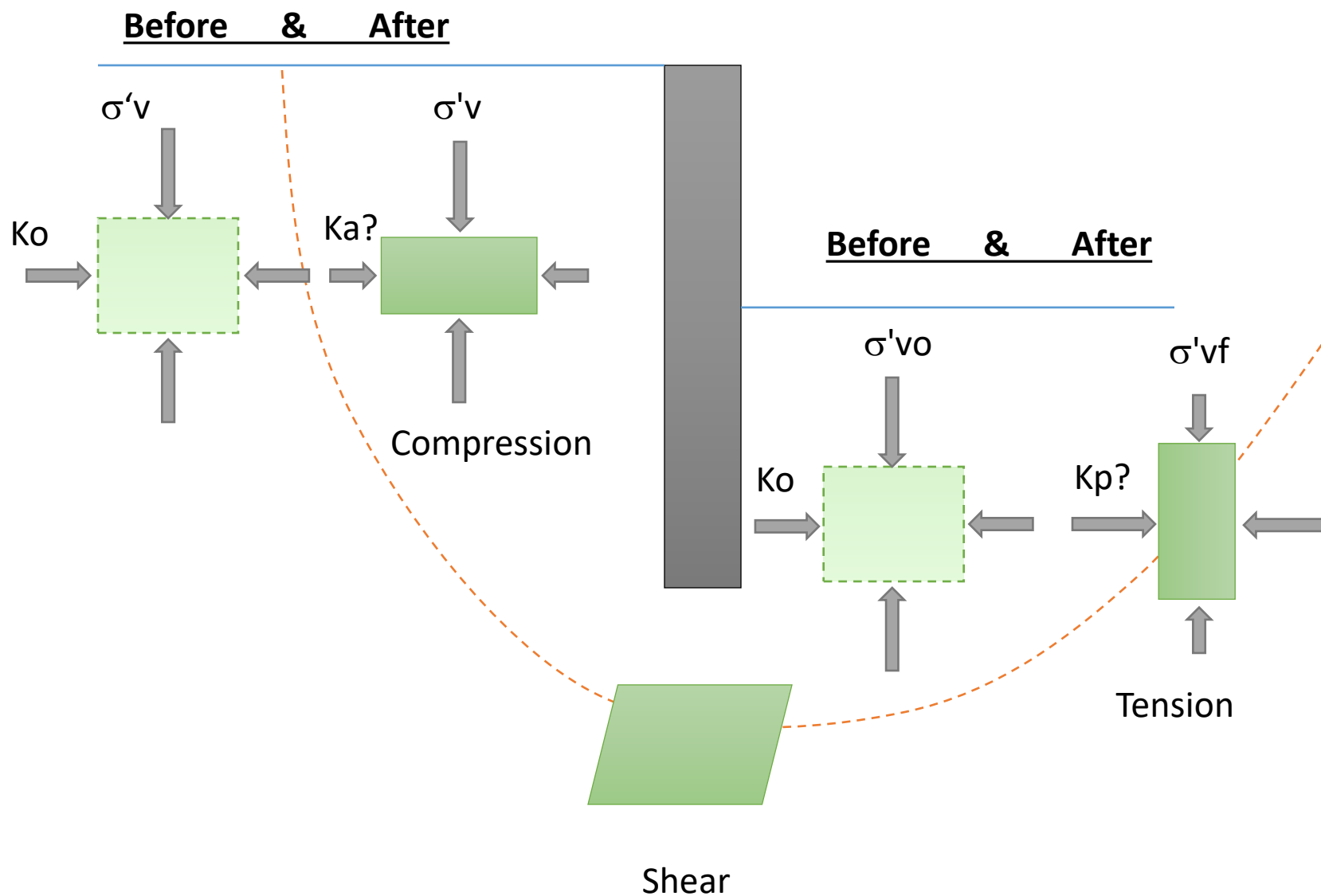
- Three clay samples are taken from the same depth. They were tested in the lab and the following strengths were reported:
 - $c' = 800$ psf, $\phi = 10$ degrees



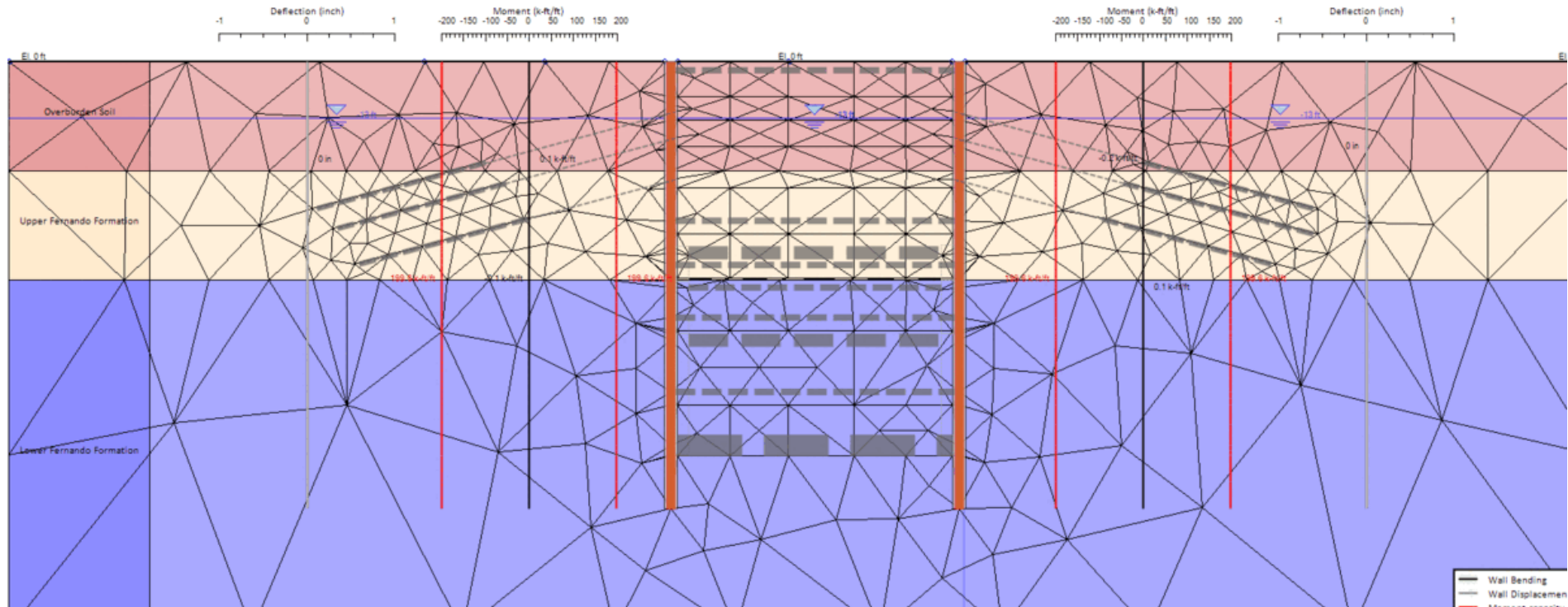
Clay Example

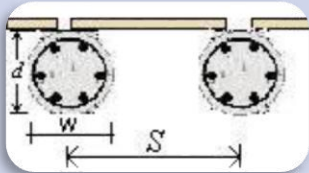
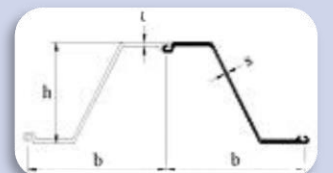
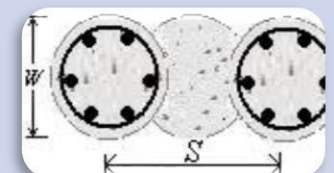
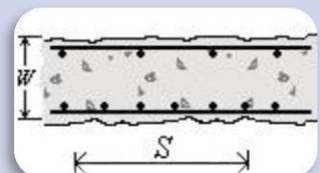
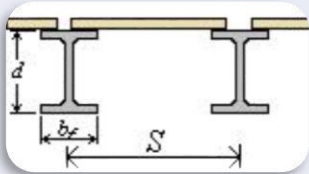
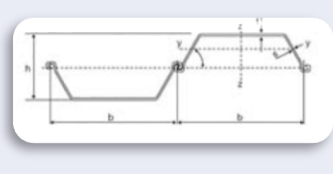
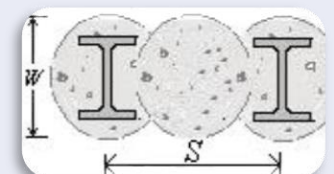
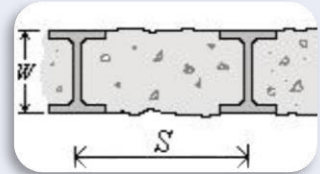
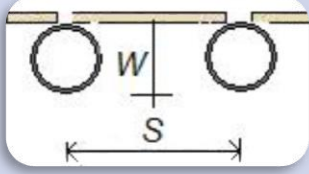
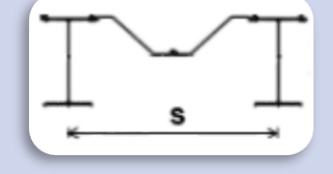
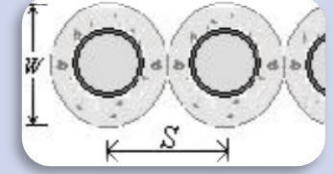
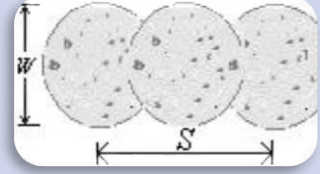
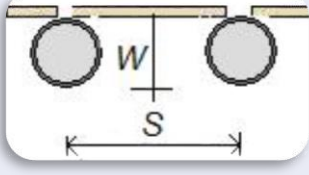
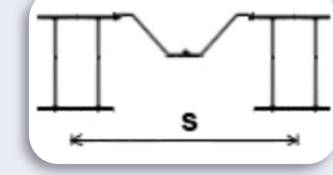
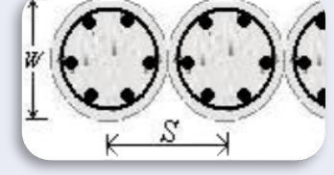
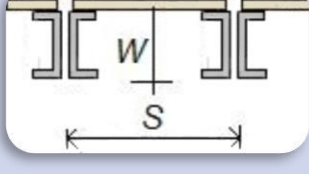
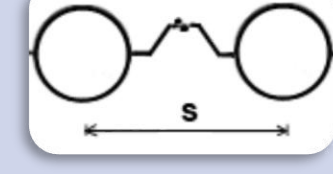
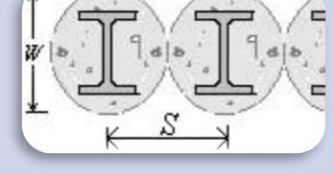
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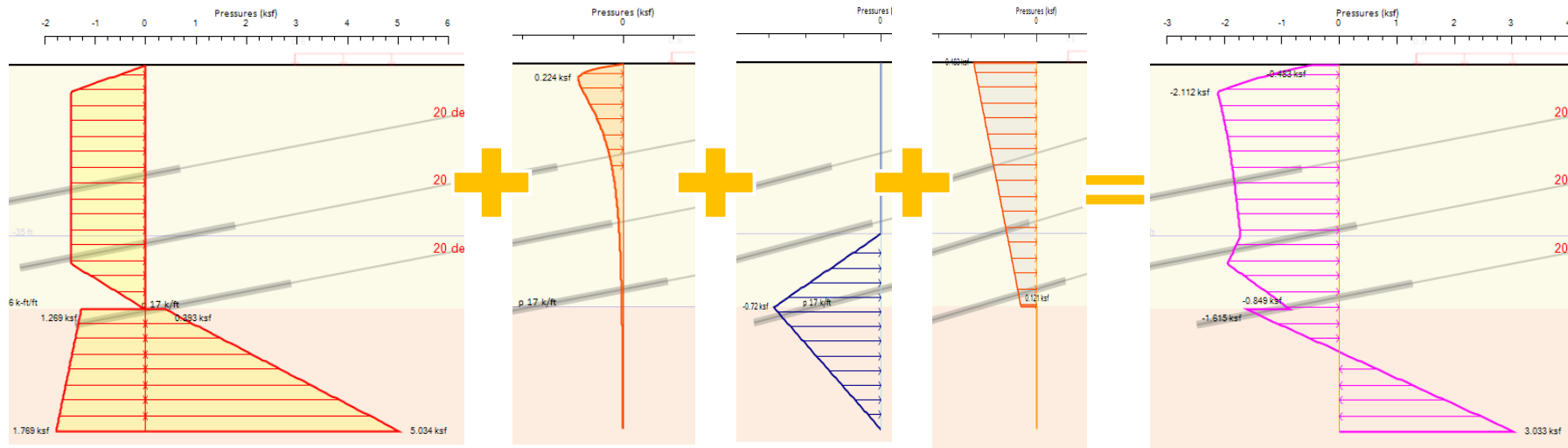


- Deep excavations always require staged construction.
- Even wall construction can affect performance.
- Start from at-rest conditions (or before)



Soldier pile walls	Sheet piles / Combined walls	Secant/Tangent piles	Slurry walls SPTC, Soil Mix, etc
			
			
			
			Jet grout
			Ground freezing

Determine net loading diagram on wall



Soil pressures

Surcharge

Water

Seismic

Net loading

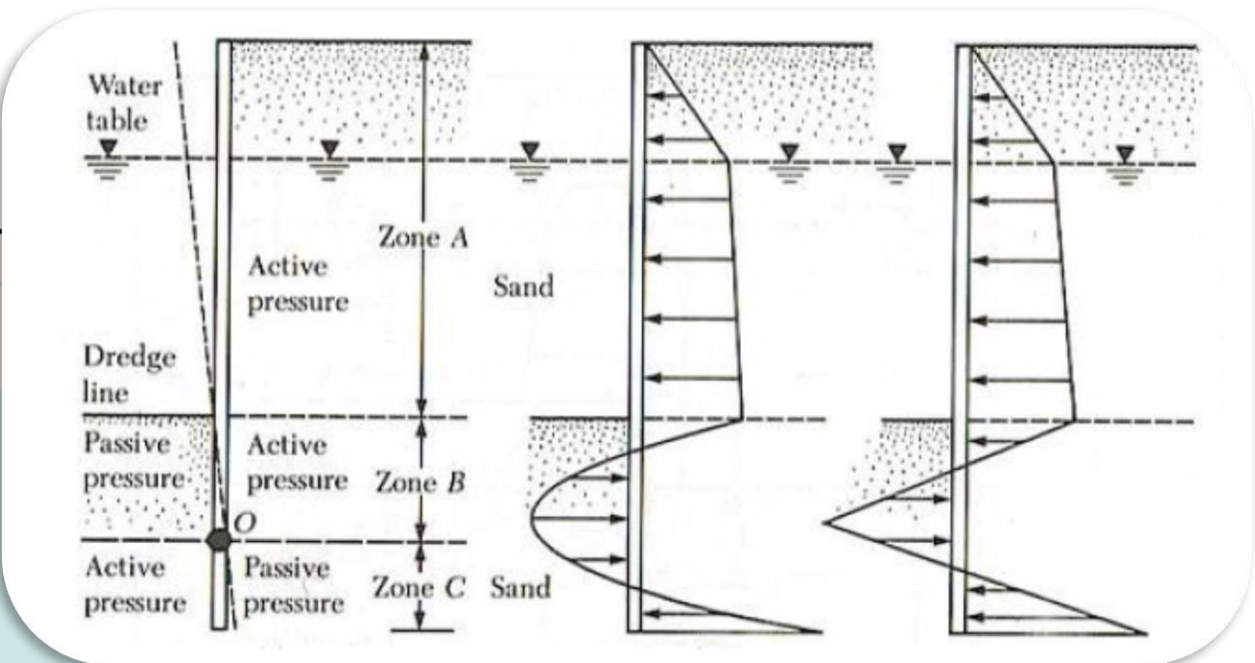
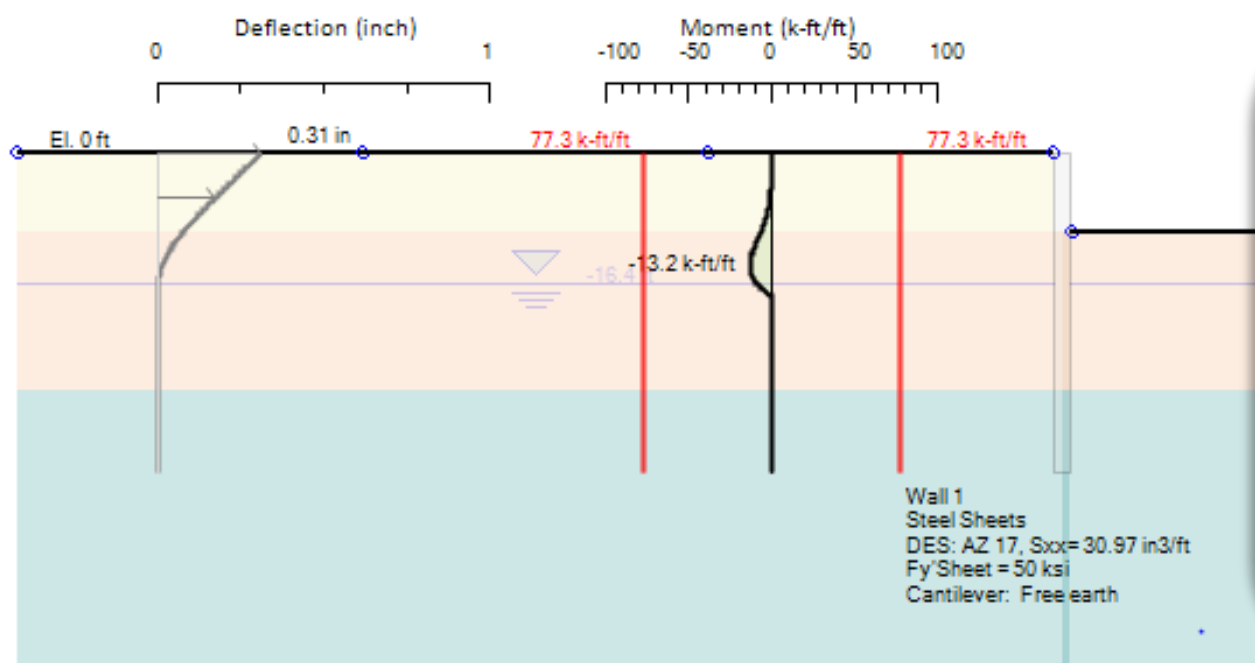
Soldier pile walls (berlin type), 3D effects

Pile spacing above excavation,

Active and passive effective widths, Water width

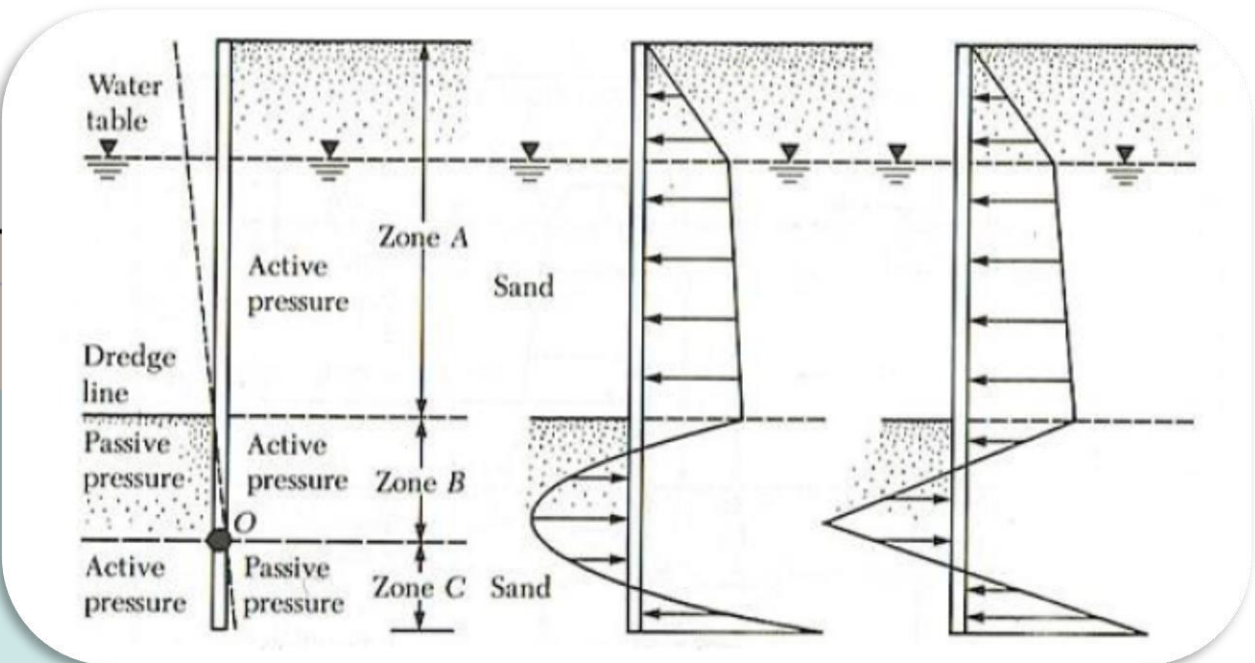
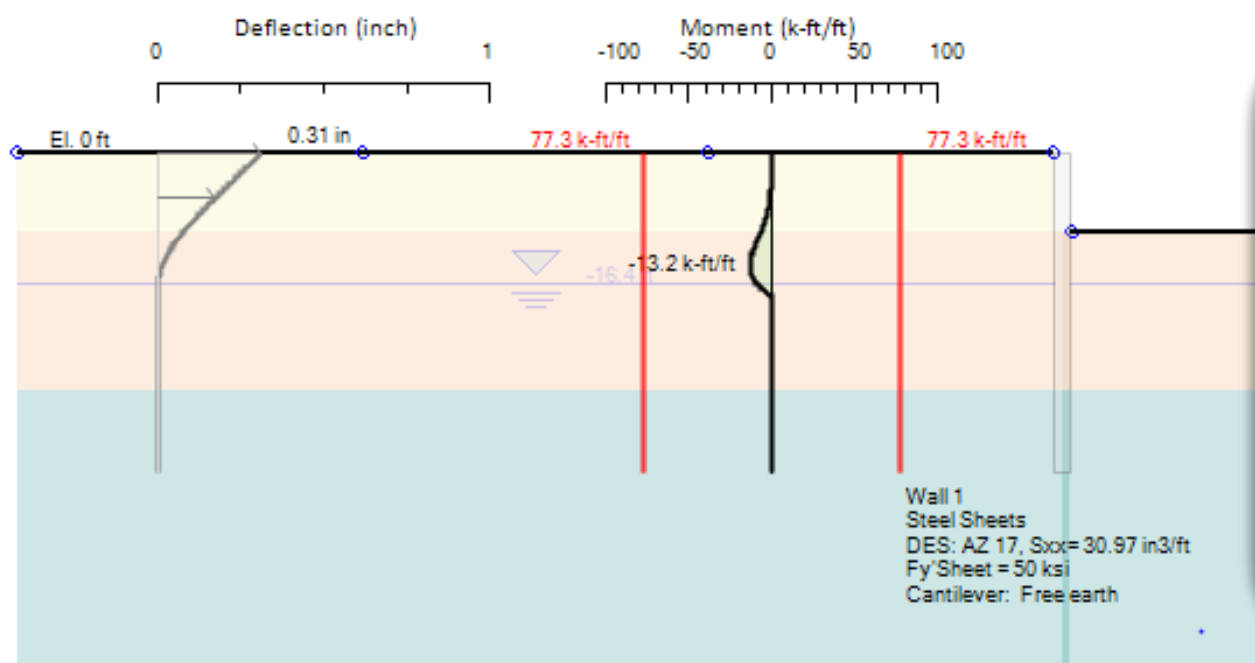


Cantilever excavation

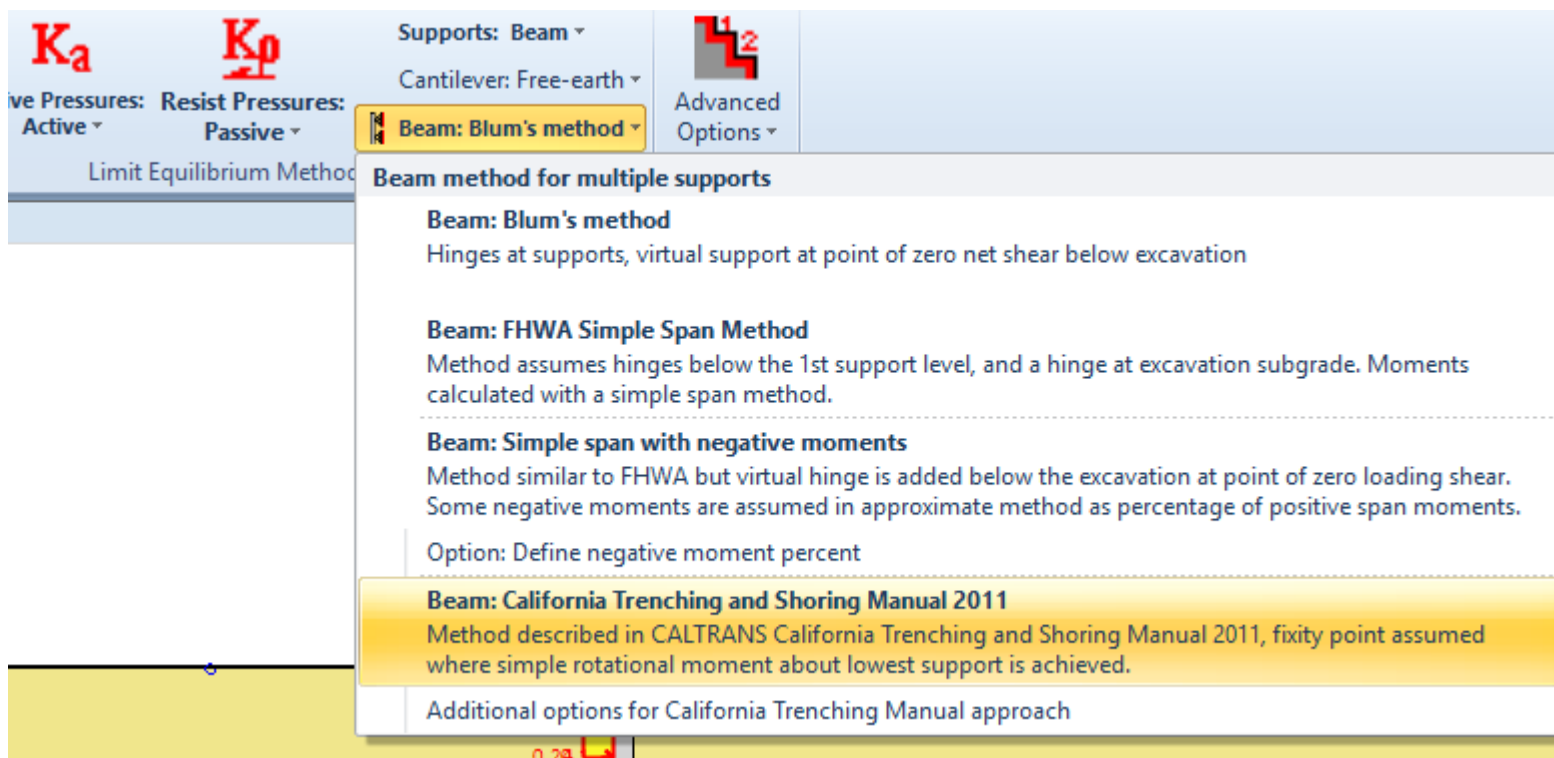




Cantilever excavation



- Use CALTRANS approach for more reasonable cantilever displacements



12.6.4 DUE TO STRIP LOAD (NO YIELDING WALL)

Similarly, Boussinesq's solution due to a strip load (Figure 12.30) is doubled to get lateral stress on a non-yielding wall as:

$$\sigma_h = \frac{2q}{\pi} [\beta - \sin\beta \cos(2\theta)] \quad (12.45)$$

where angles β and θ are defined in Figure 12.30.

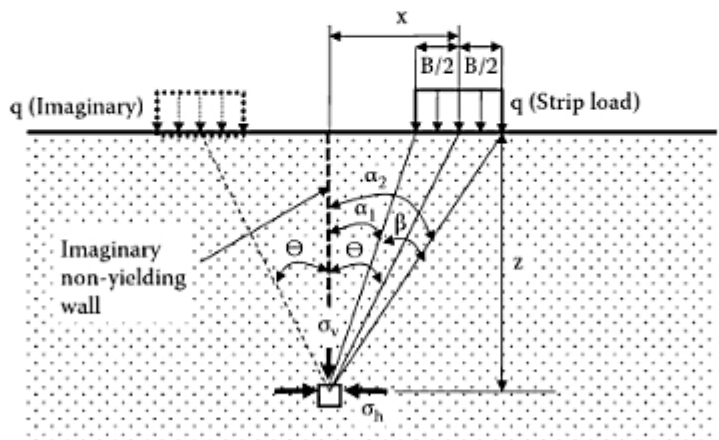
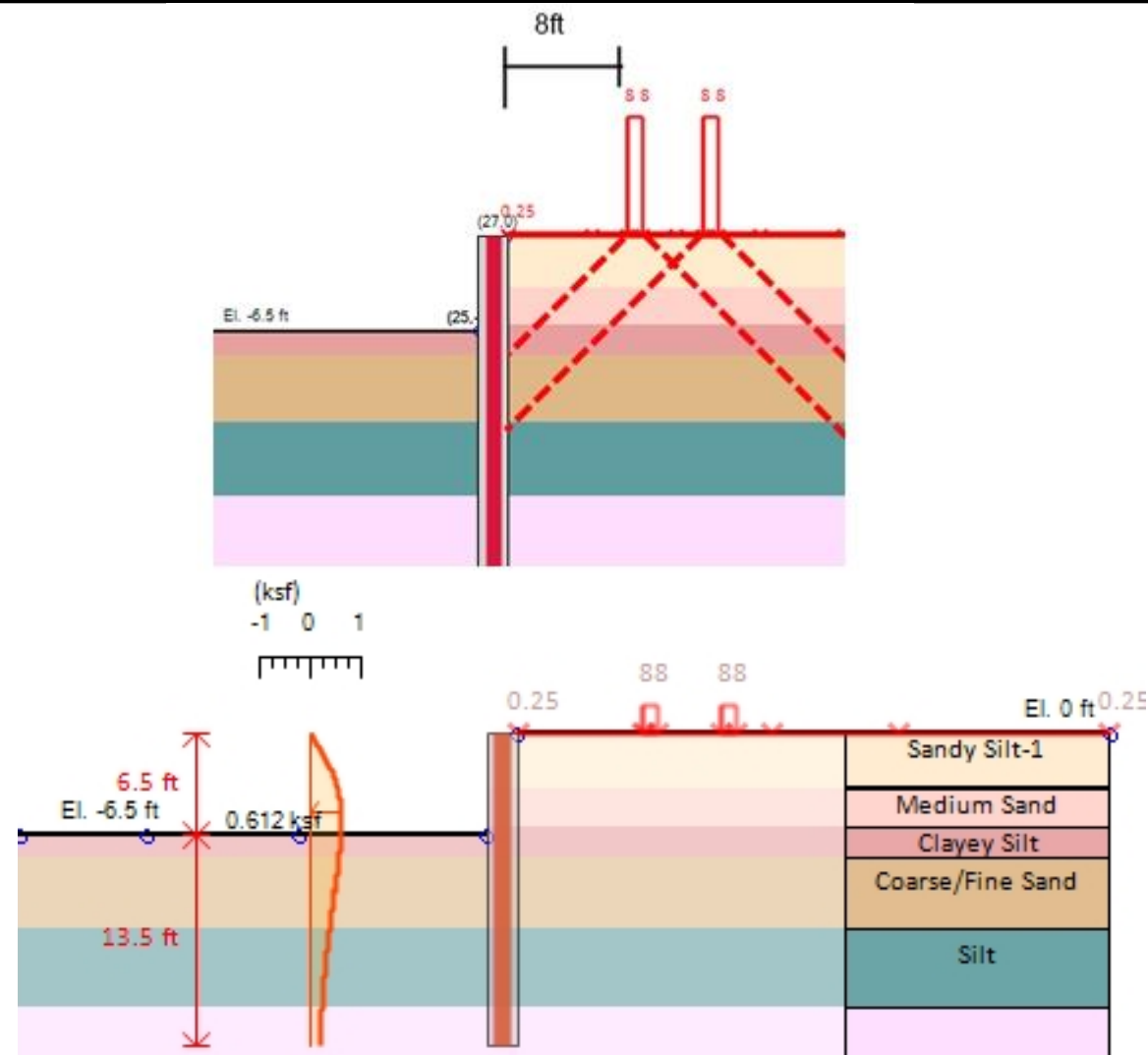
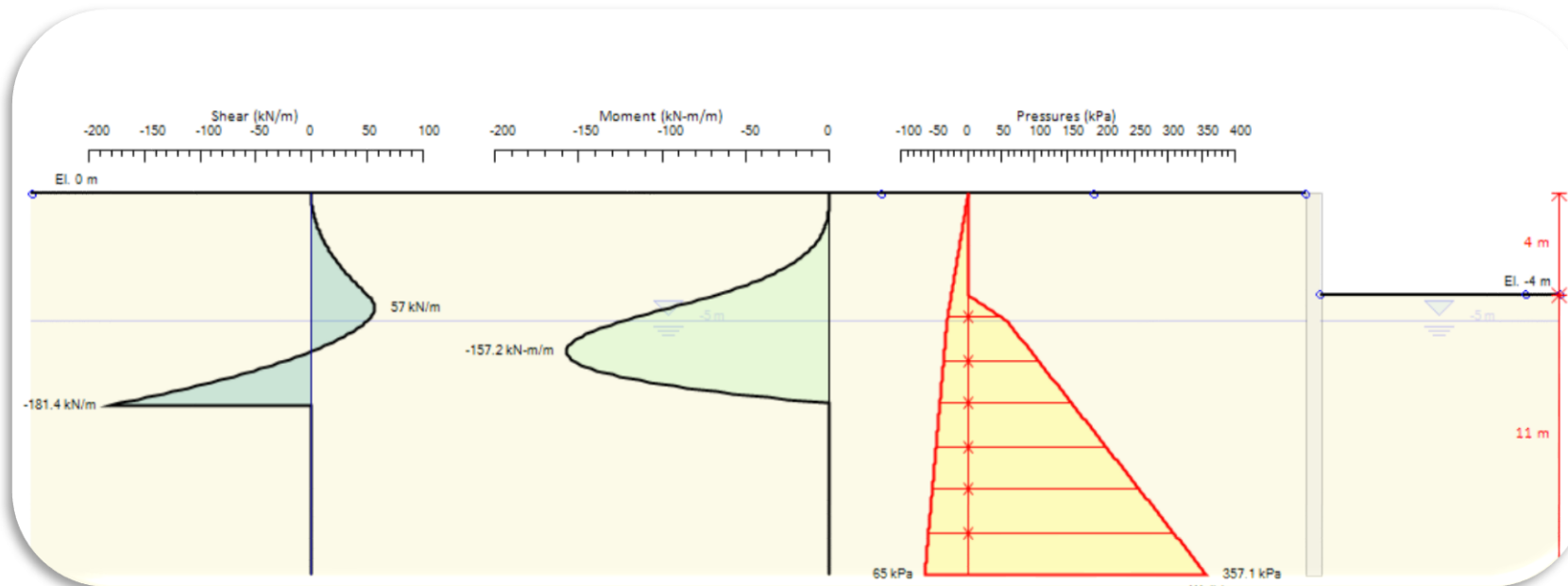


FIGURE 12.30 Boussinesq's lateral stress against nonyielding wall due to strip load.

Figure 1: Excerpt from "Soil Mechanics Fundamentals"



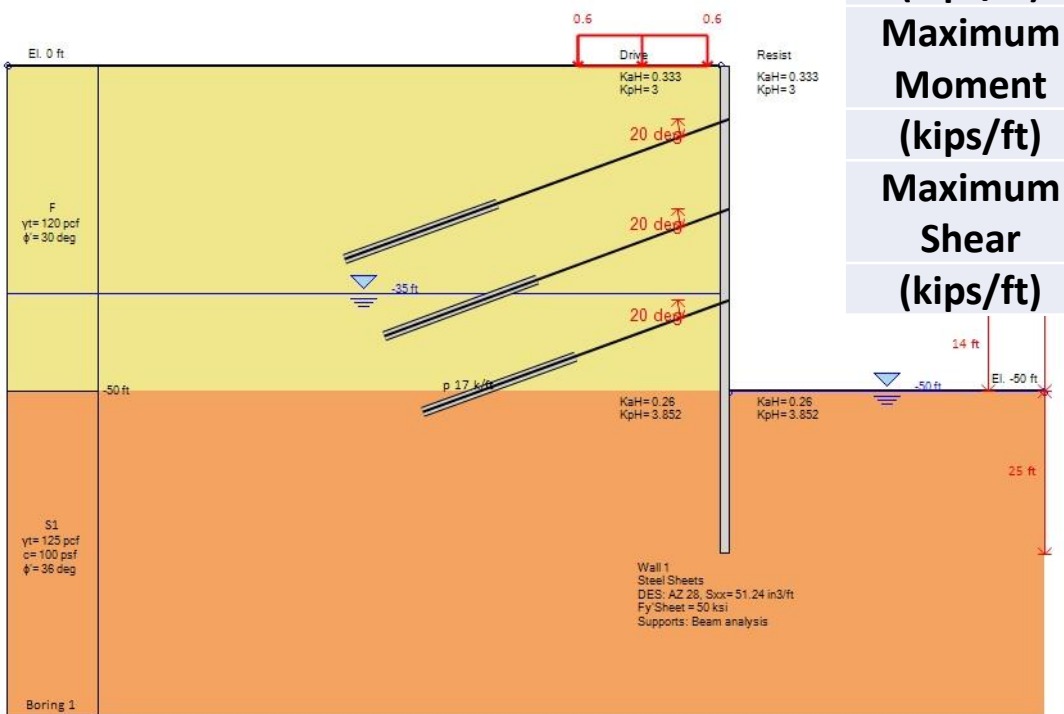
Balances out moment
 Shear not balanced
 Increase length by 1.2 to get FS 1.0
 Then apply additional safety factors





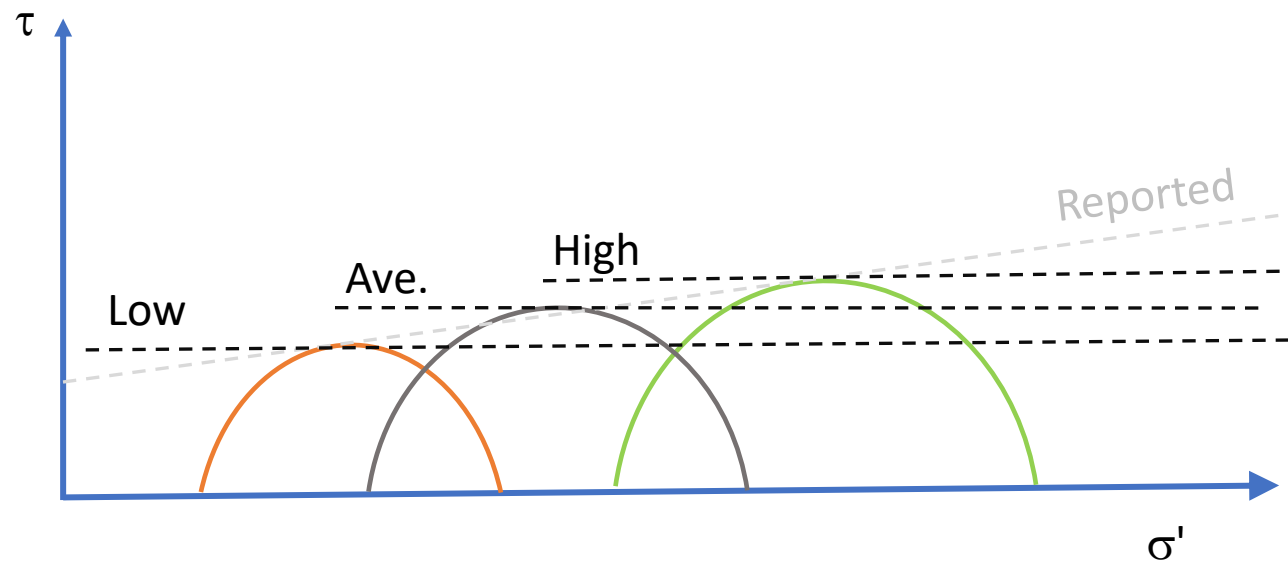
Static loading final excavation (50 ft exc.)

	Blums's method	FHWA Simple span	FHWA Mixed Blum	CALTRANS Method	CALTRANS - negative	Nonlinear analysis*
Maximum support reaction (kips/ft)	33.68	23.91	27.66	30.08	30.08	30 – 31.8
Maximum Moment (kips/ft)	58.25	36.78	74.29	99.41	87.45	65 – 86
Maximum Shear (kips/ft)	18.13	13.14	15.49	17.77	17.77	17.4 - 20

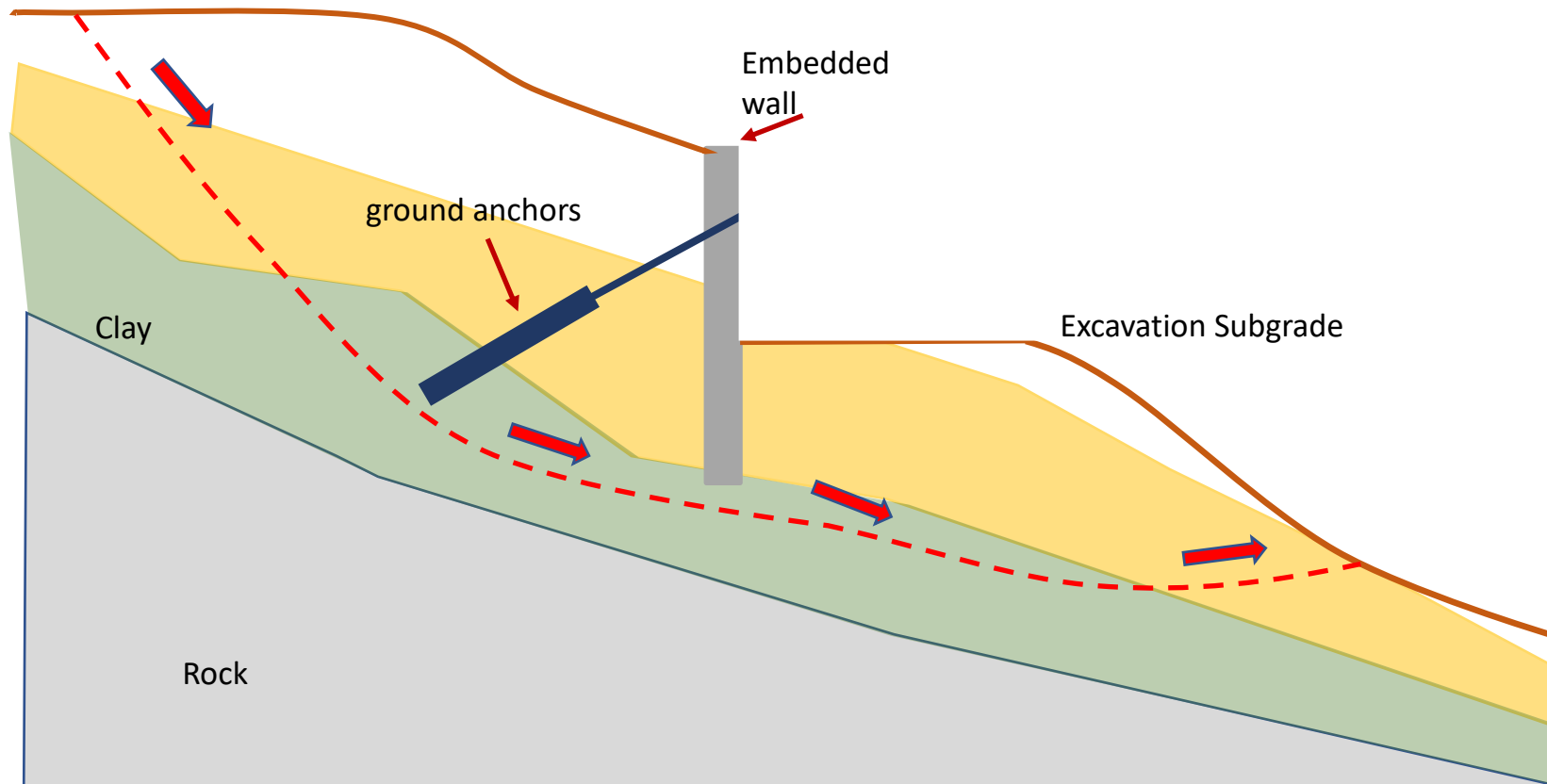


Clay Example

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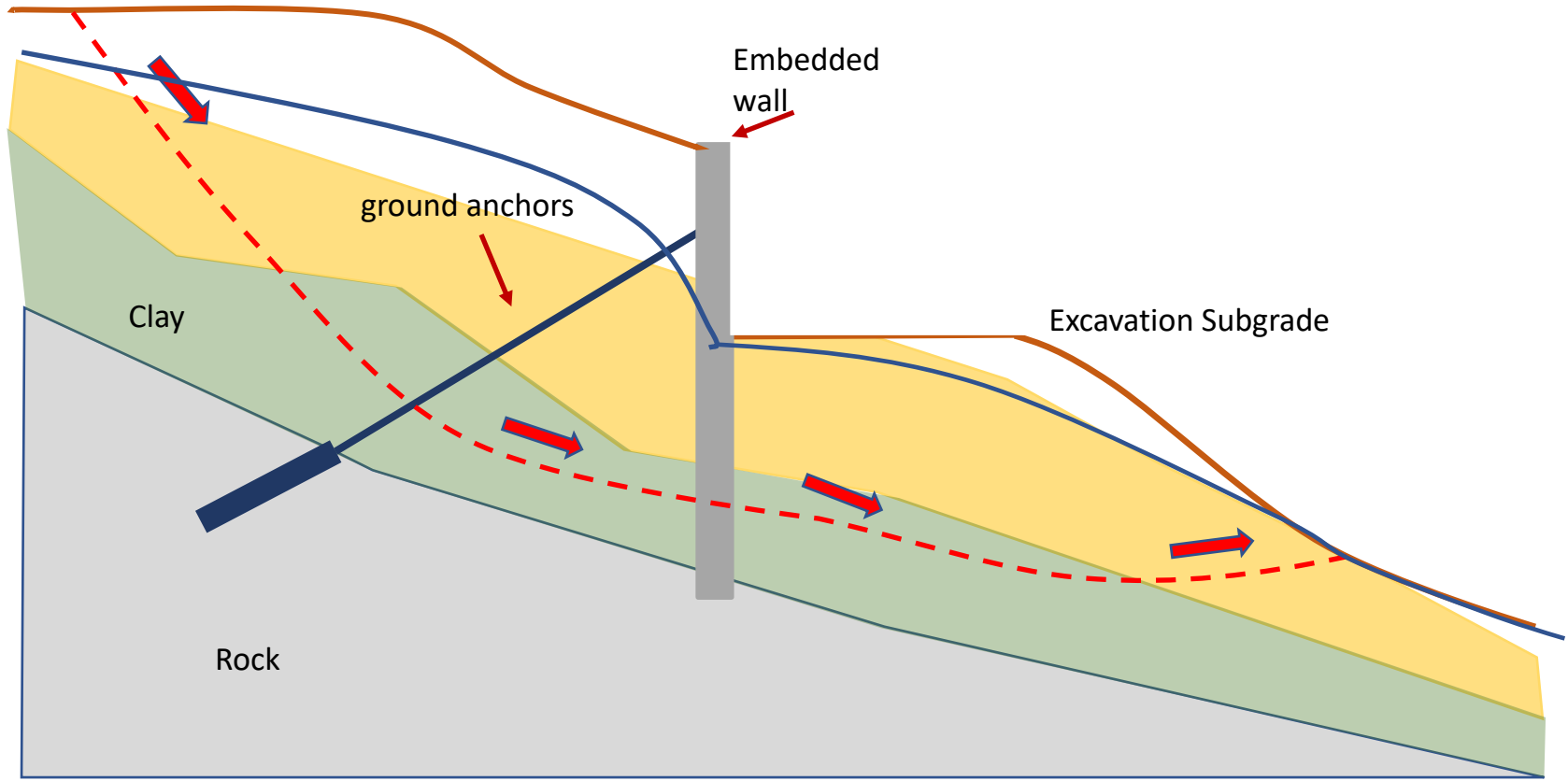


- Traditional active and passive pressures are based on active and passive wedges.
- In slopes, many times, sliding mass is far beyond a simple wedge





SLOPE STABILIZATION

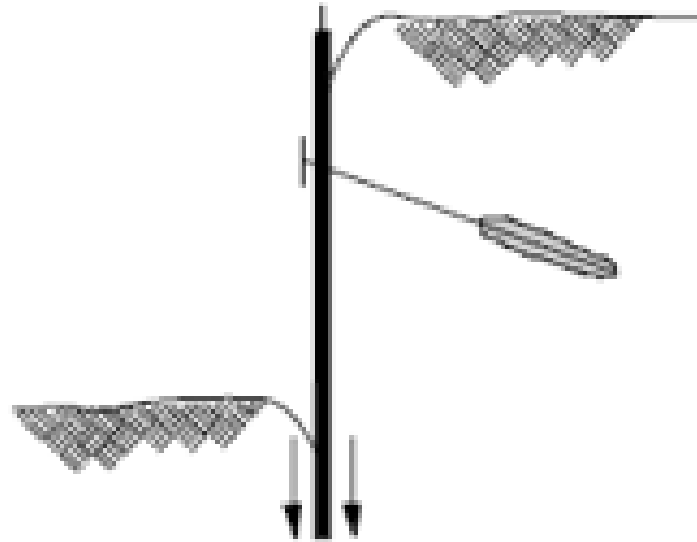


AXIAL WALL FORCES

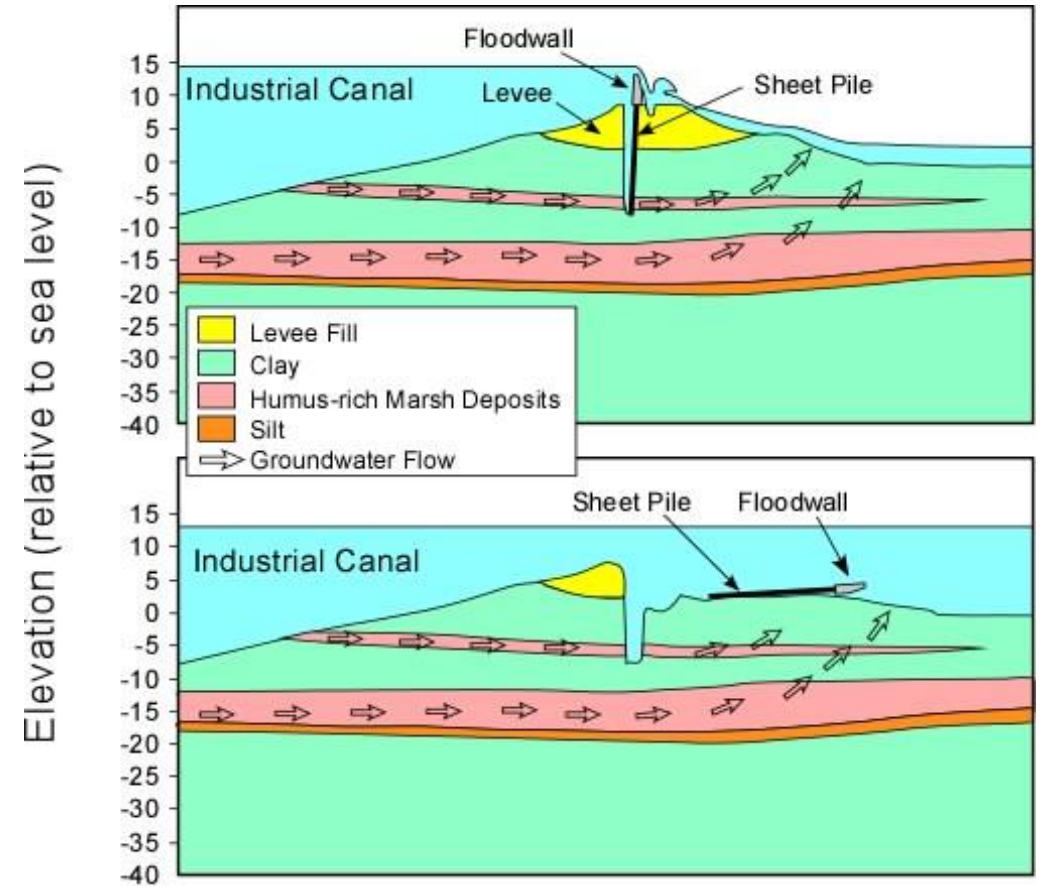
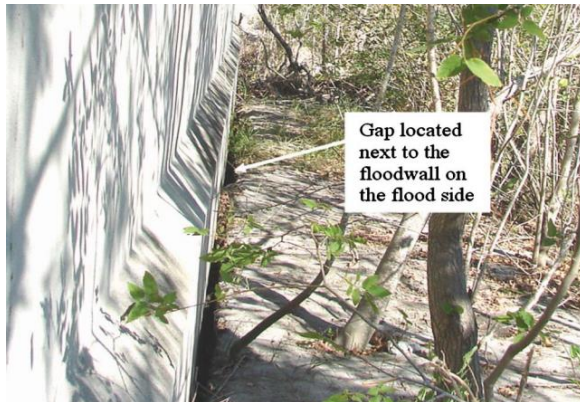
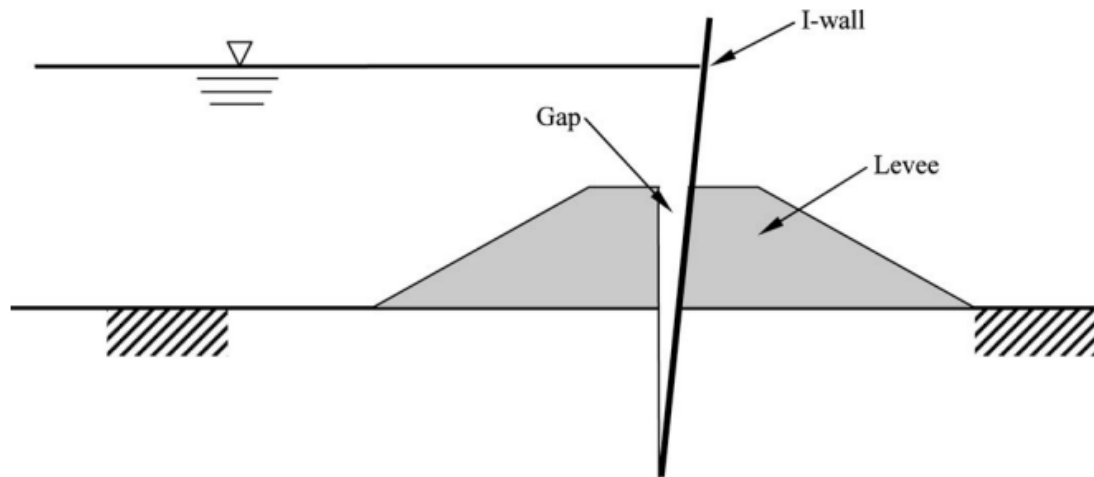
Ignoring axial forces on wall

Imposed by steeply inclined tiebacks

Wall does not have sufficient geotechnical pile resistance below excavation

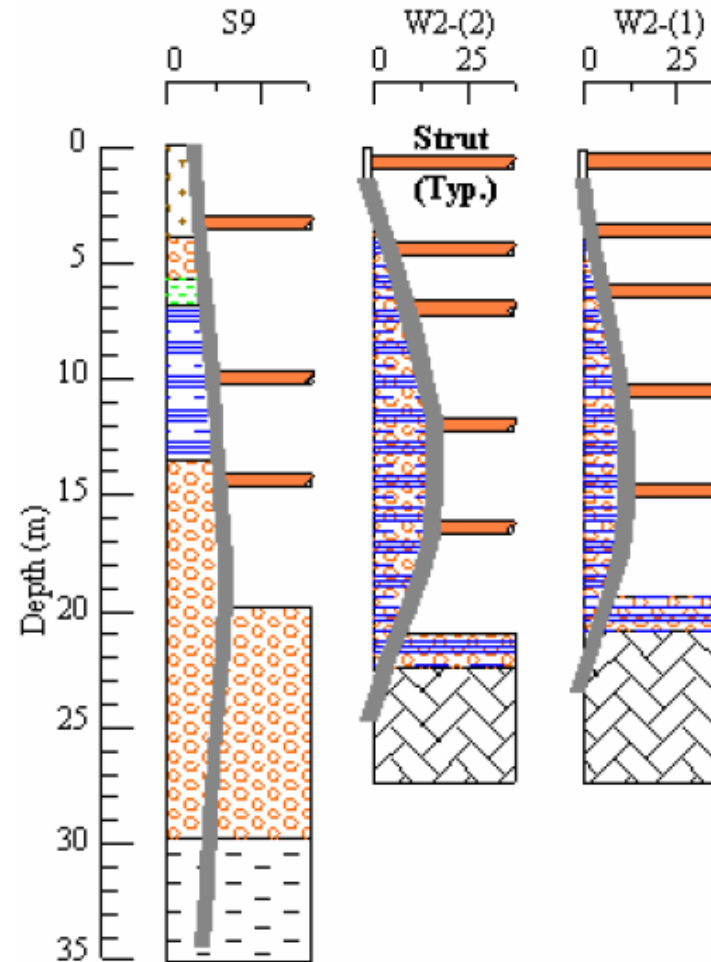


17th Street Canal Breach Area

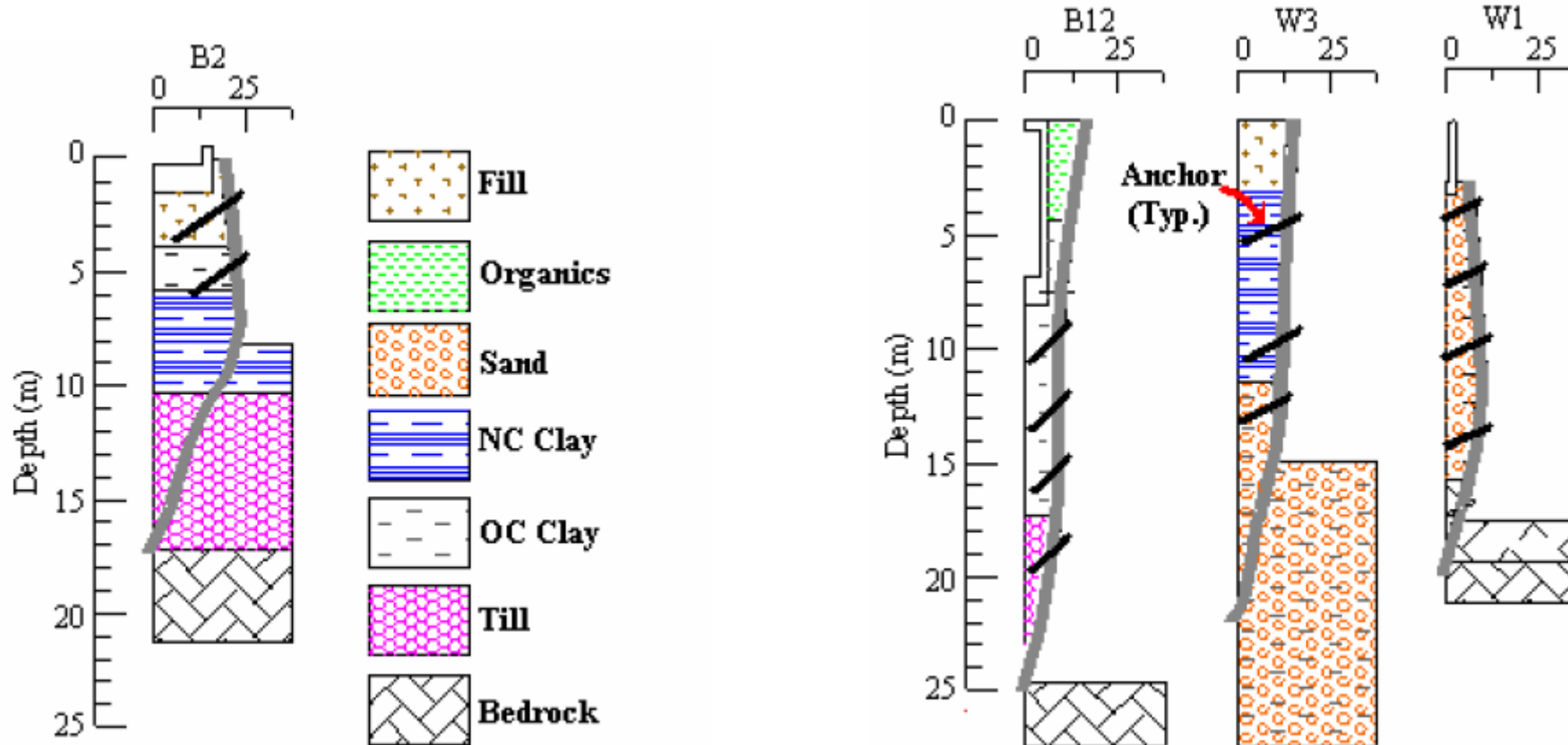


Reference: Prof. Stephen A. Nelson, Tulane University

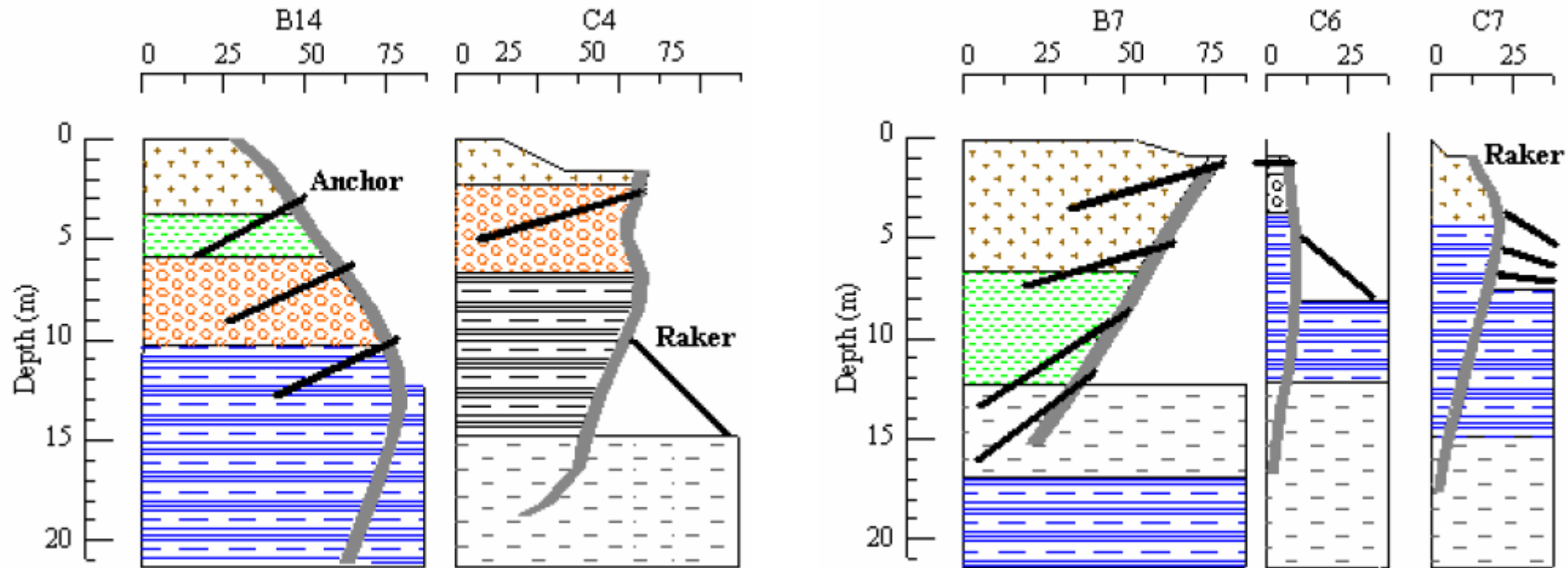
- Struts transfer forces, but usually not prestressed
- Displacements accumulate on every stage
- Embedment into stiff stratum (rock makes a difference)



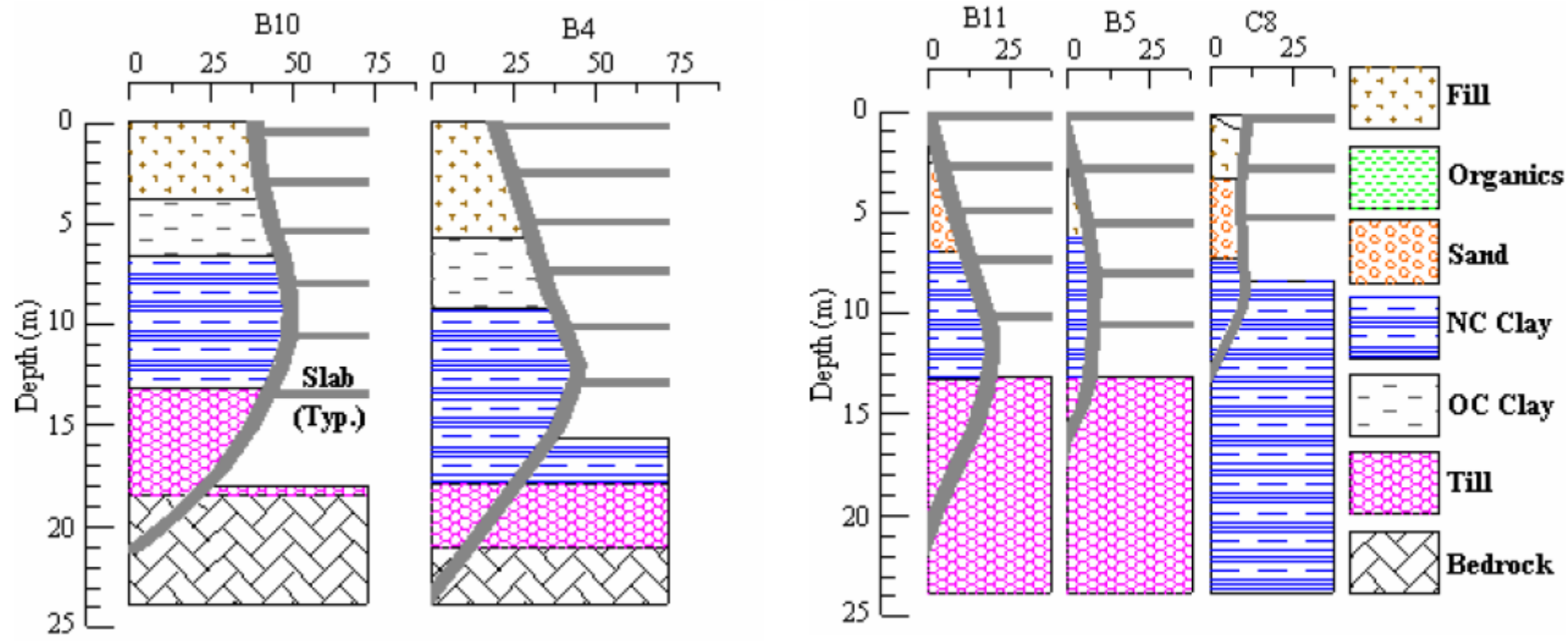
- Wall base does not move



- Basal movements add to wall displacing at bottom
- Ground anchors in zone of movements



- Concrete has tendency to shrink



- GIGO (Garbage in – garbage out)
- Wall is wished in place
- It is good to know what to expect!
- Small strain stiffness vs. large strain
- Basal heave and cantilever displacements usually overestimated
- Surface settlements occasionally are out of touch (models without anisotropy)
- Nice colors can give a false sense of assurance

- 3ft diaphragm wall (0.9m)
- Up to 92 ft excavation
- Buildings on two sides

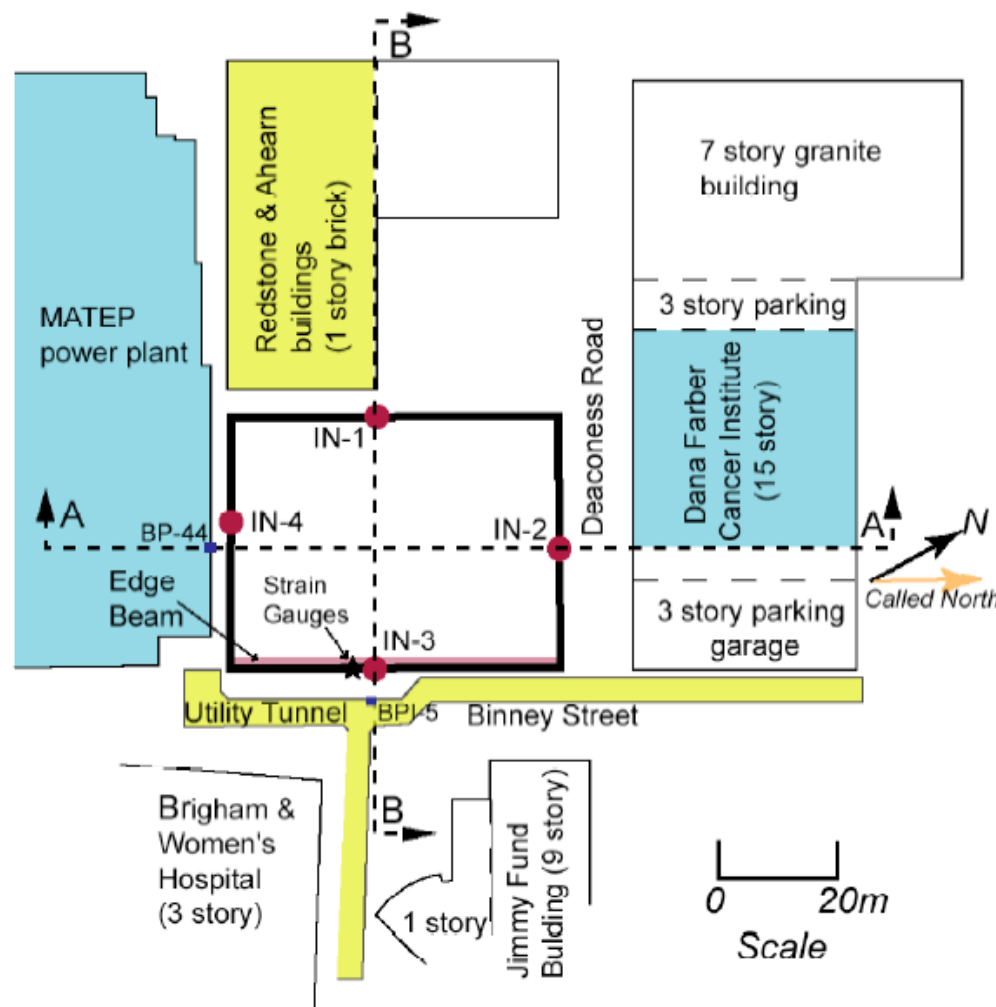
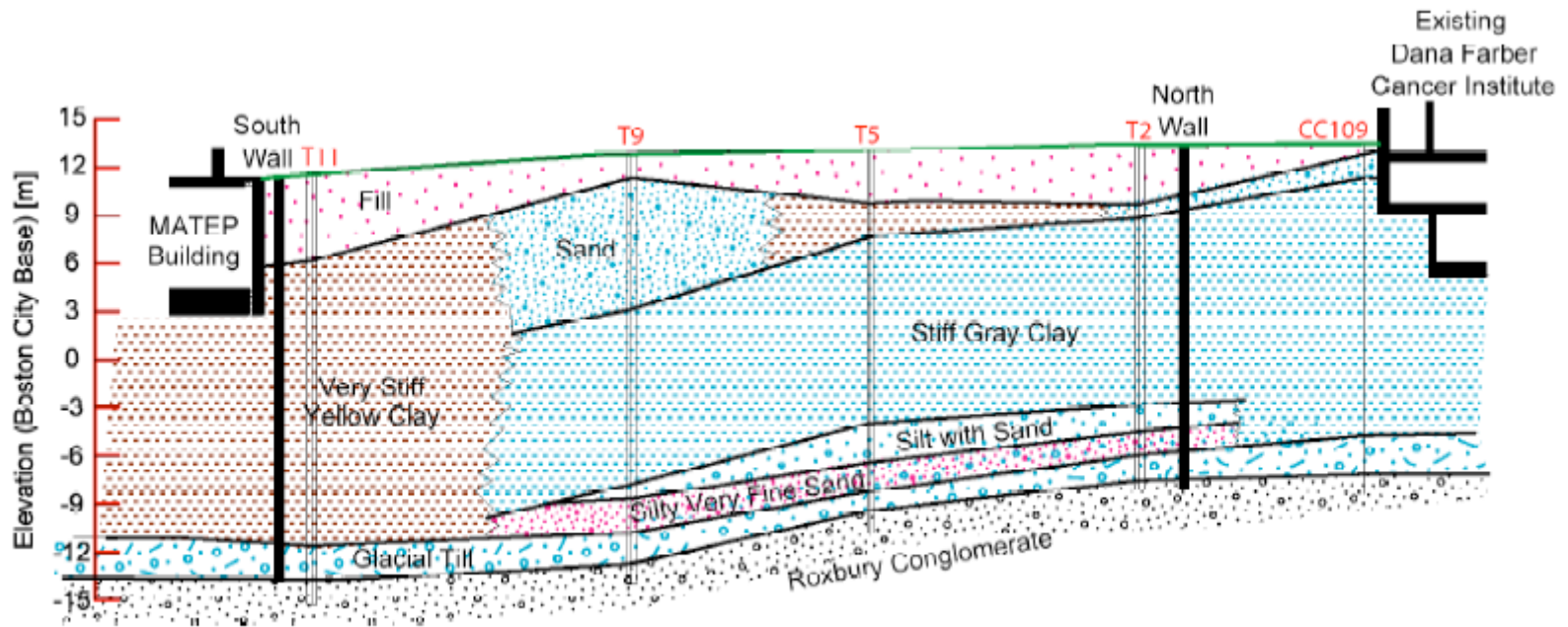


Fig. 1. Dana Farber research tower site plan



Cross Section

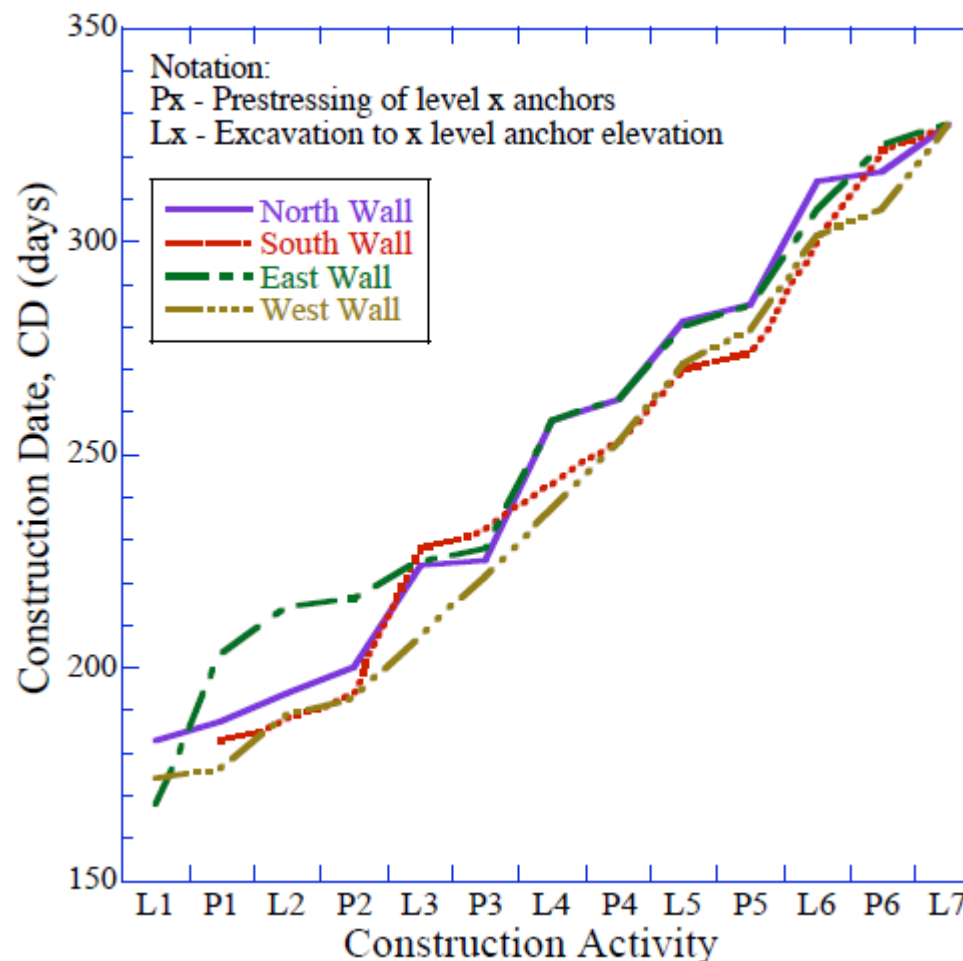


a) Cross-section A-A



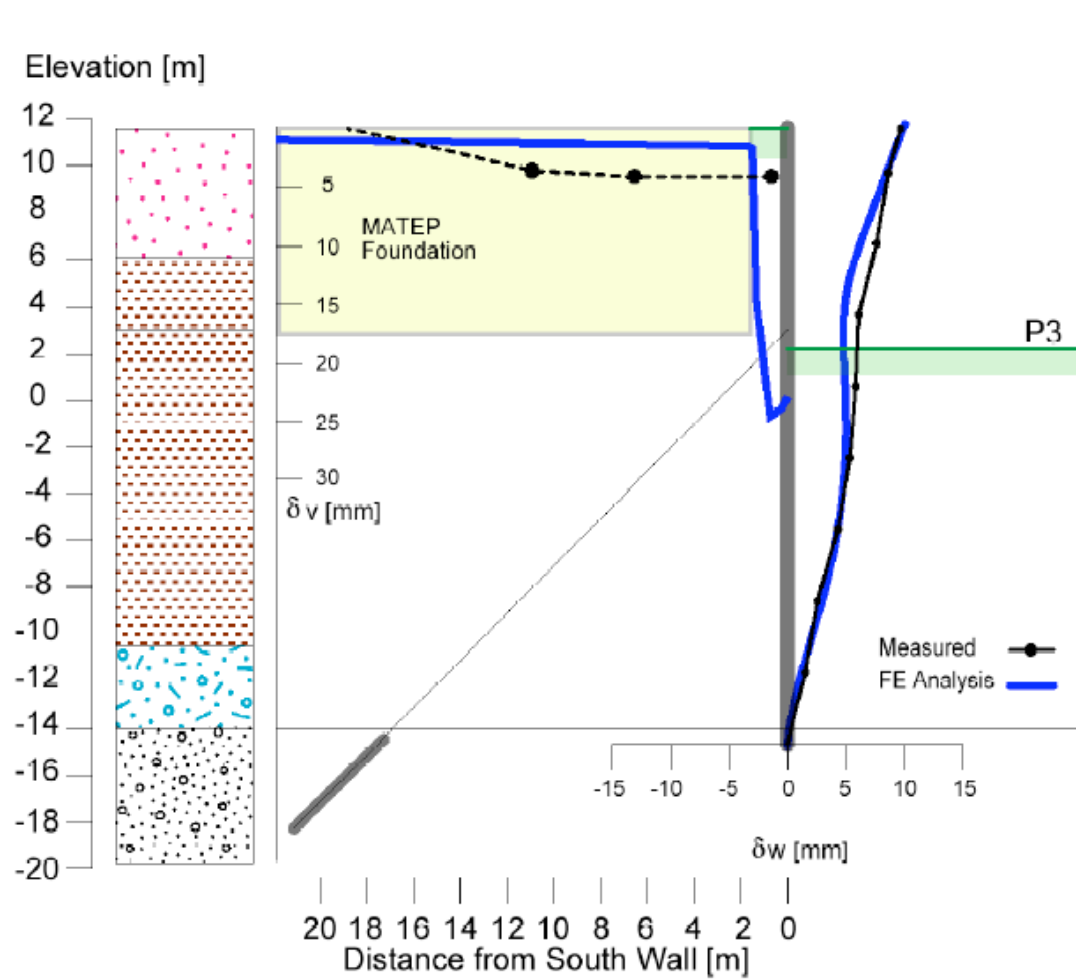
Anchor	Parameter	North	South	East	West
P1	EA ($\times 10^3$ kN/m)	0.79	--	0.016 ²	0.79
El. 9.0m	L_f (m)	24.4	--	--	32.9
	F_L (kN/m)	385	--	250 ²	397
P2	EA ($\times 10^3$ kN/m)	0.96	--	0.96	0.96
El. 5.9m	L_f (m)	20.1	--	25.0	28.0
	F_L (kN/m)	435	--	426	438
P3	EA ($\times 10^3$ kN/m)	1.66	1.08	1.66	1.66
El. 2.9m	L_f (m)	15.9	24.4	20.7	23.8
	F_L (kN/m)	795	510	1349	829
P4	EA ($\times 10^3$ kN/m)	2.04	1.45	2.04	2.84
El. -0.2m	L_f (m)	11.6	19.5	16.7	19.5
	F_L (kN/m)	965	695	1052	1486
P5	EA ($\times 10^3$ kN/m)	1.14	1.95	1.14	2.30
El. -3.3m	L_f (m)	7.0	15.2	12.2	15.2
	F_L (kN/m)	550	905	820	1024
P6	EA ($\times 10^3$ kN/m)	1.14	2.72	1.14	2.30
El. -6.3m	L_f (m)	4.6	11.0	7.9	9.1
	F_L (kN/m)	550	1135	867	1310

Notes: 1. F_L – lock-off load,
 L_f – estimated free-length of anchor
 2. Edge beam installed at ground surface (Fig. 1).

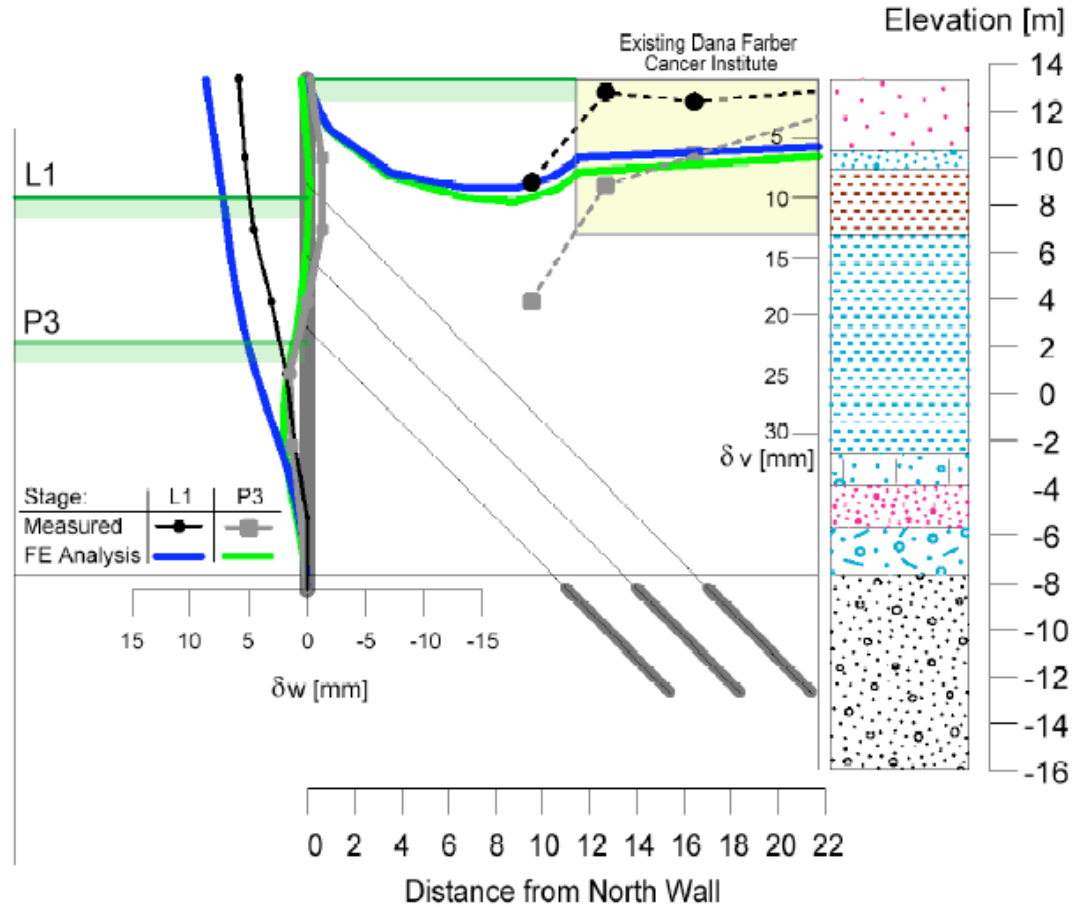




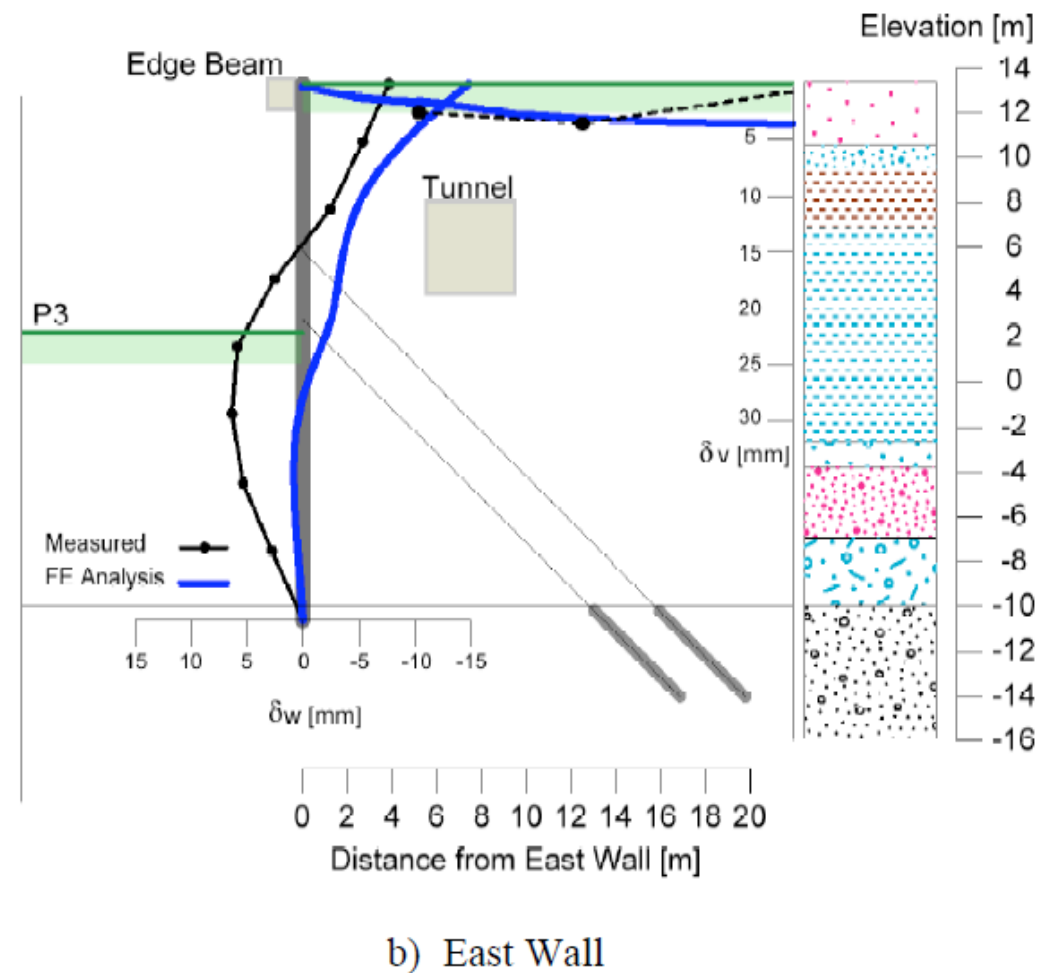
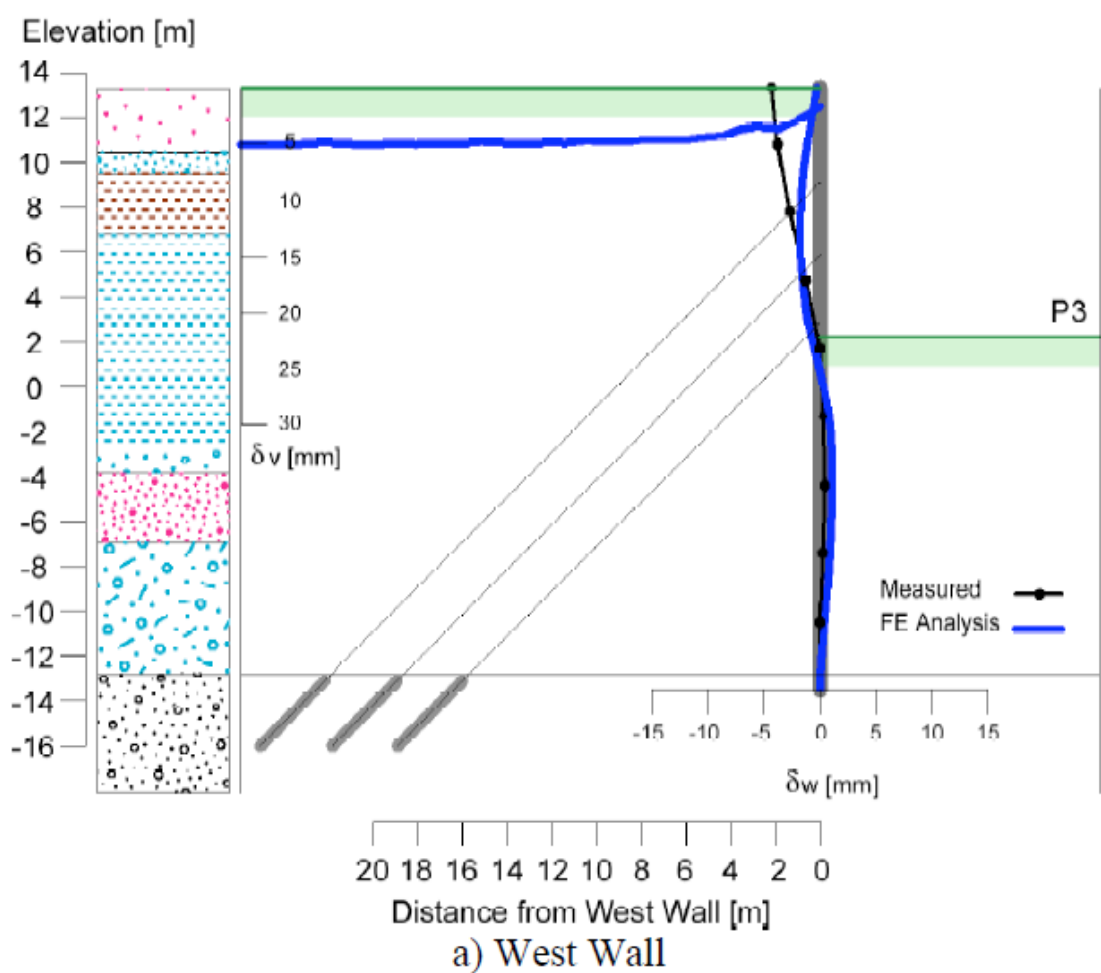
Section A-A Early Results

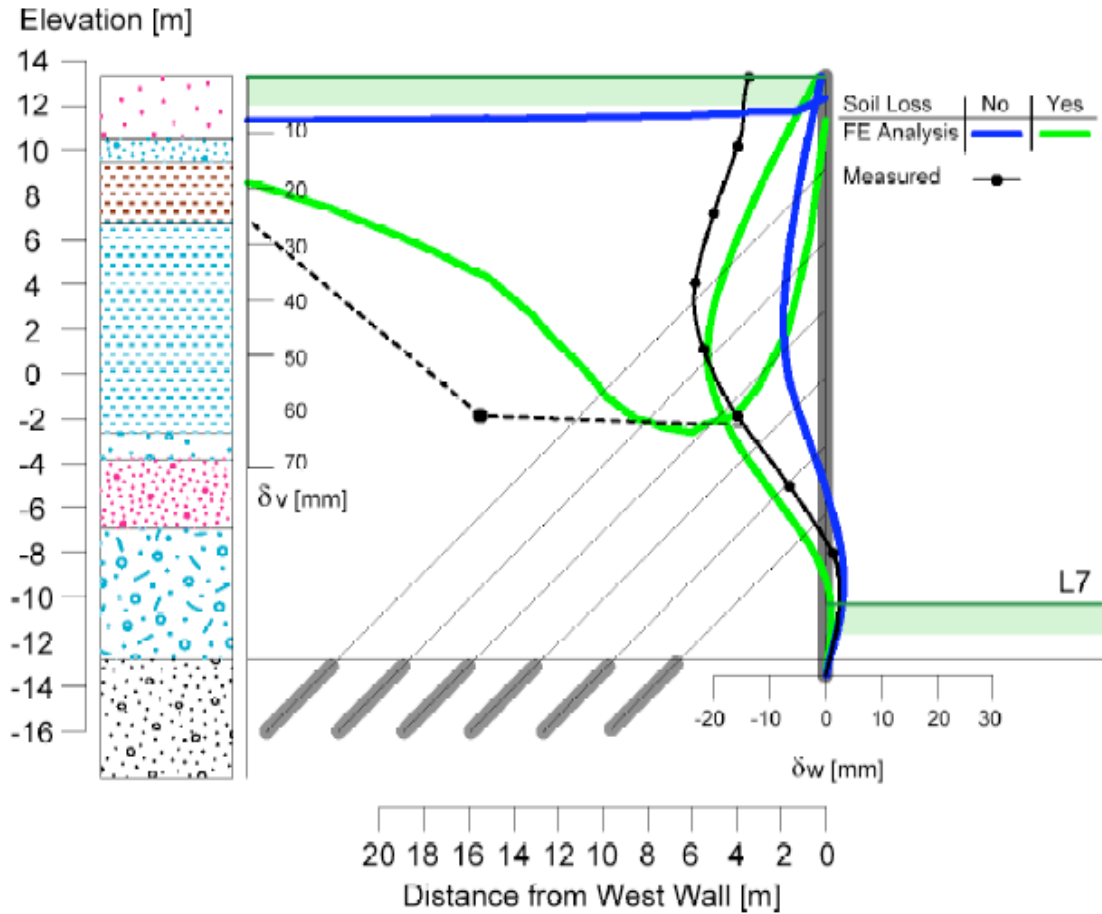


a) South Wall

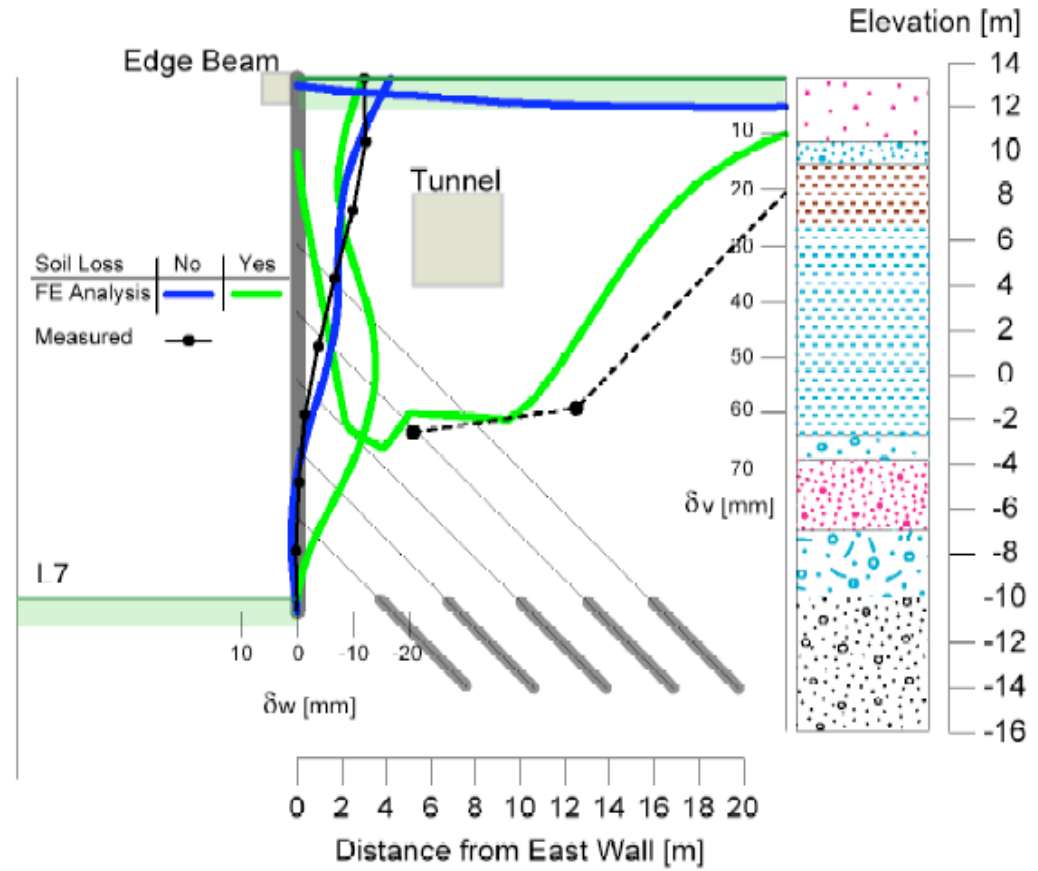


b) North Wall





a) West Wall



b) East Wall

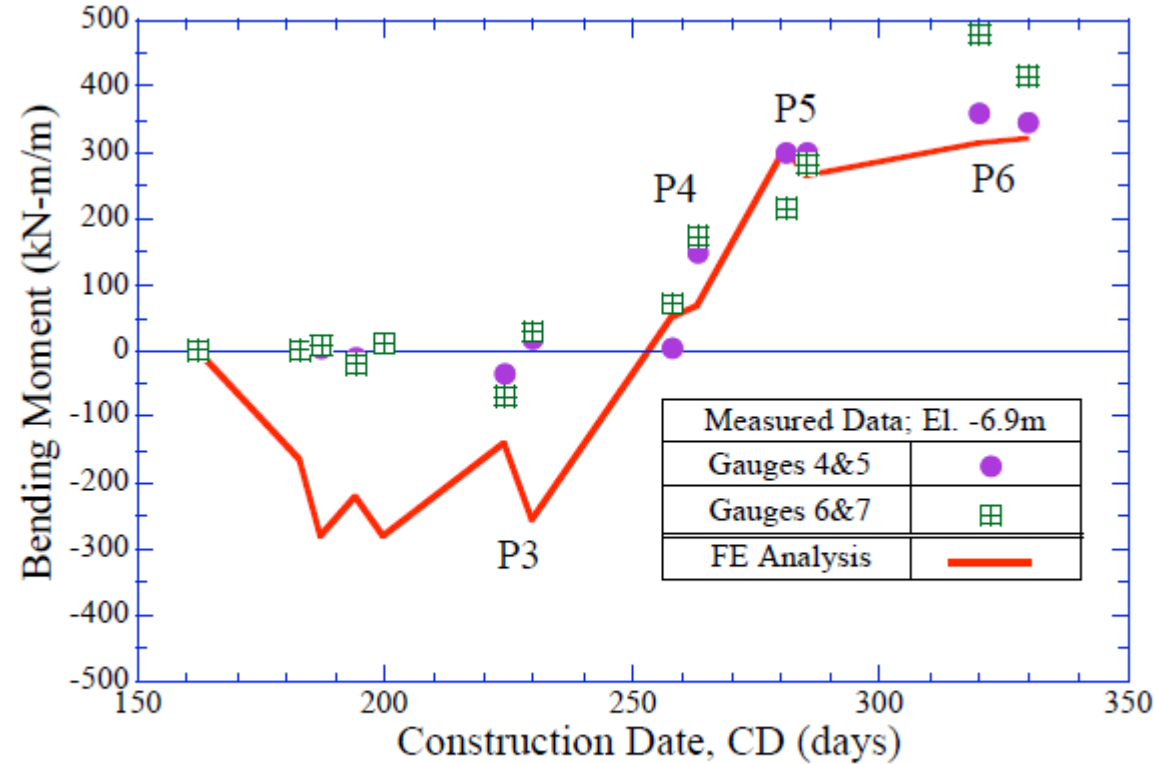


Fig. 9 Comparison of computed and measured bending moments in North wall



- Extremely difficult if not impossible to create perfect match
- Construction effects could not have been foreseen in regular design but played major role in actual performance
- Bending moments may be even more challenging to match
- Settlements were more difficult to match than horizontal displacements



- Deep excavation design complexities
- **Numerous items that might have to be considered**
- DeepEX software gives a number of warnings and diagnostics, about 200 checks!
- Good engineering judgement still rules!